



September 21, 2023

The Corporation of the Town of Fort Erie  
1 Municipal Centre Dr.  
Fort Erie, Ontario, L2A2S6

**1127 Garrison Road, Fort Erie**  
**Functional Servicing Report (Revised)**

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***1.0 Background & Information***

***1.1 Introduction***

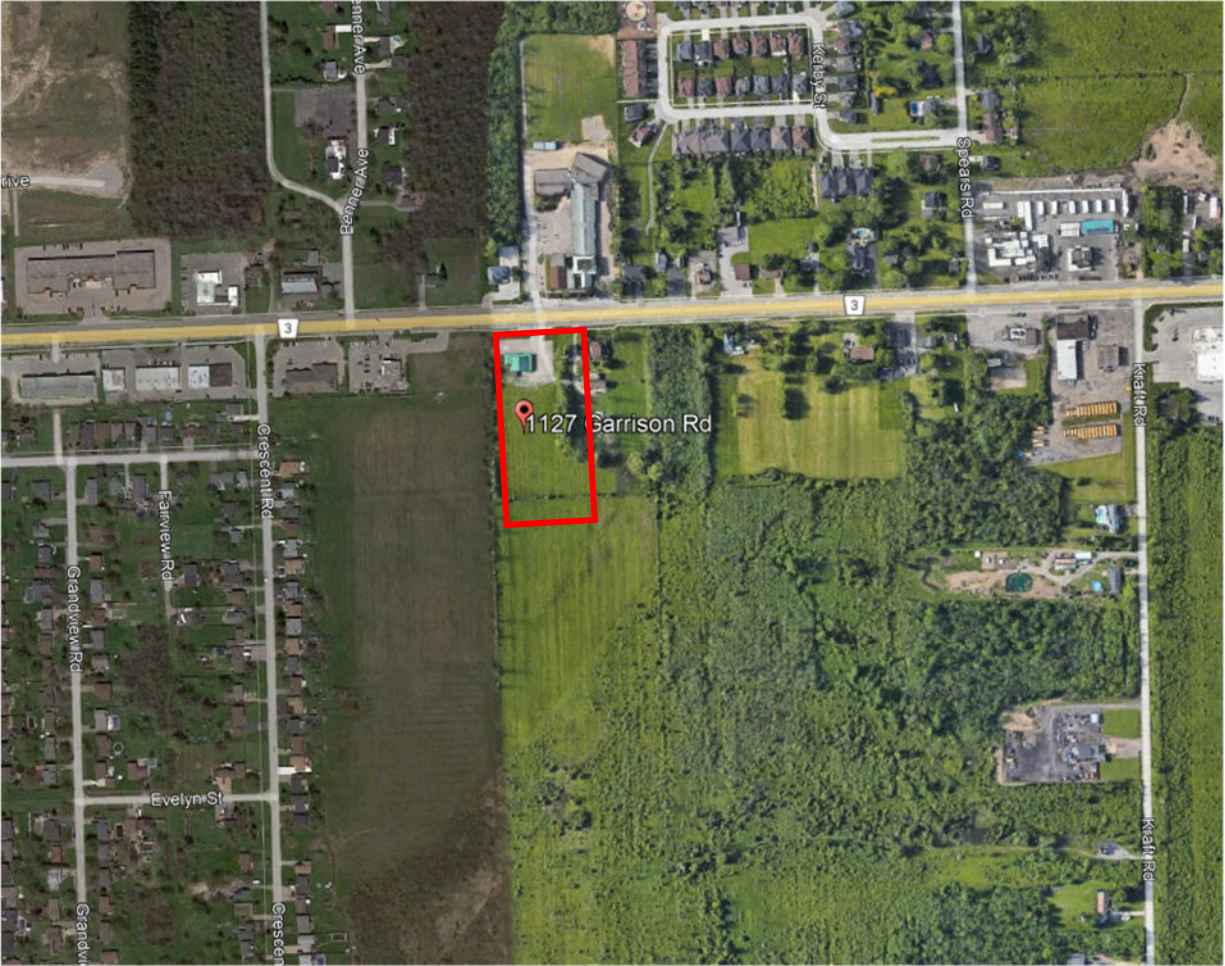
LandSmith Engineering & Consulting Ltd. have been retained by TrinityStar Aquila Inc. for the completion of a Functional Servicing Report in support of Re-zoning and Official Plan amendment applications for the lands located at 1127 Garrison Road in the Town of Fort Erie. A pre-consultation for the property was completed by NPG Planning Solutions in spring of 2022 on behalf of the owner, and the City's comments were provided through the planner as per the meeting of May 12<sup>th</sup>, 2022.

The purpose of this Functional Servicing Report is to review the existing municipal services currently in place and available for the servicing of the 90 new units on Garrison Road and ensure their suitability for the proposed Re-zoning and Official Plan Amendment applications. In addition, this report will address the local Stormwater Management (SWM) context for the lot and the required stormwater quantity and quality control measures.

***1.2 Site Location & Proposed Development***

As noted above, the site being analyzed is located at 1127 Garrison Road, in the Town of Fort Erie. The property is located approximately between Crescent Road and Kraft Rd on the south side of Garrison Road. The lot is currently designated Commercial and Urban residential and zoned Highway Commercial (C3), Neighbourhood Development (ND), and Environmental Conservation (EC).

The current proposal is for the redesignation and rezoning of the land to permit residential uses. This is illustrated on the Concept Plan prepared by Organica Studio + Inc. which is attached to this report within Appendix 'A' for reference purposes. As can be seen, the existing building is to be removed, being replaced by four proposed blocks consisting of one mixed use (commercial and residential) block and three residential blocks, totalling 90 units. The site location plan below further illustrates the location of the proposed development in the context of the local Fort Erie area.



**Figure 1: Site Location Plan**

**2.0 Servicing Analysis**

**2.1 Water Servicing:**

There is a 300mm diameter watermain on Garrison Road as indicated on the Plan & Profile drawing for Garrison Road from Fort Erie Infrastructure Services, which is contained within Appendix ‘E’ for reference purposes.

Fire-flows have been calculated for each of the new residences according to the methodology recommended by the Ontario Building Code. Using this method, the required fire-flow was calculated to be 45 L/s. Given the 300mm diameter of the existing watermain on Garrison Road it is expected that this fire-flow can be provided. Details of the fire-flow calculation are contained within Appendix ‘B’ for reference together with a Fire Protection Sketch which illustrates the setbacks of the proposed buildings from the nearest adjacent units.

In addition to the fire-flow calculations, domestic water-use calculations for each of the buildings was completed based on the number of units proposed and the expected number of fixtures for each unit. Based on the Fixture Unit Method as outlined in OBC Table 7.6.3.2.A it is expected that the required peak instantaneous domestic use flow rate for the site will be 9.77 L/s.

A water service size of 150mm can be utilized to provide both the required domestic flows and fire-flows. A Preliminary Servicing Plan has been attached to this report for reference purposes within Appendix 'B' and this plan illustrates the proposed location of the water service and the connection point to each building. It is expected that each building will be sprinklered for additional fire protection, however these details will be finalized at the site-plan stage.

## **2.2 Sanitary Servicing:**

There is a 450mm sanitary sewer on Garrison Road. The site will be connected to the 450mm sanitary sewer with a 200mm sanitary pipe entering the property on the north side of the property. Each of the four blocks will be serviced via a 150mm diameter service connections as illustrated on the Preliminary Servicing Plan contained within Appendix 'B' for reference purposes.

The expected sanitary generation rates for the site have been calculated using the Region of Niagara Standard rate of 275 Liters per capita per day. Based on the proposal for 90 units it is expected that the population for the development will be approximately 180 person (3 persons / unit).

Based on this population the expected peak sanitary generation rate from the site will be:

$$(275 \text{ L/cap/day} \times 270 \text{ persons}) / (24 \times 60 \times 60) = 0.859 \text{ Liters / Second}$$

Peaking Factor = 4.098 (Harmon Formula)

**TOTAL PEAK FLOW = 3.52 Liters / Second**

The areas contributing to the local sanitary sewer are described within the Region of Niagara Water/Wastewater Master Servicing Plan (WWMSPP, 2016) Figure 4.H.1 which has been included within Appendix 'B' for reference purposes. Based on the areas contributing to the existing 450mm sanitary sewer on Garrison Road it is expected that there will be ample capacity within the conveyance system for the proposed density of the development.

The proposed development site is within the catchment of the Alliston Avenue Sanitary Pumping Station (SPS). The Alliston Avenue SPS is noted to have an operational firm capacity of 43 L/s while experiencing an average dry-weather flow of 5.8 L/s (in 2016). It should be noted that the SPS was experiencing high stormwater infiltration and that the peak wet-weather flows were above the

operational firm capacity in 2016. This SPS was expected to be upgraded due to growth triggers and is noted within the Niagara Region WWMSP to be upgraded with a pump replacement to increase the firm capacity of the station between 2022-2031.

Relevant pages from the WWMSP are included in Appendix 'B' for reference purposes – further discussion should be carried out with the Region to determine whether this upgrade would be required at the present time. It appears that the domestic flows can be accommodated within the SPS under its current condition, however stormwater infiltration is using significant capacity within the station. The Town of Fort Erie has an on going wet-weather flow reduction program which may have decreased wet weather flows within the catchment.

### **2.3 Stormwater Servicing:**

The existing grades of the subject lands are illustrated on the Topographic Survey prepared by The Larocque Group and contained within Appendix 'A' for reference. This topographic survey was analyzed in order to determine the pre-development drainage pattern for the lands. A Pre-Development Drainage Area Plan was then prepared and is contained within Appendix 'D' for reference purposes. As can be seen, under the pre-developed condition the site drains almost entirely from north to south and onto the adjacent lands. There is a small intermittent swale which runs southerly on the lands of 885 Kraft Road which receives the runoff from the subject lands and conveys it further southerly toward Lake Erie. An image from the Niagara Peninsula Watershed Explorer indicating the location of this swale is included in Appendix 'D' for reference.

The adjacent infrastructure was reviewed to determine whether it would be possible to provide a storm connection from the subject lands to Garrison Road. The Plan and Profile drawing for Garrison Road indicates that there is a 450mm concrete storm sewer along the north side of Garrison Road – however review of the invert elevation of the storm sewer indicates that it is not at sufficient depth to service the subject lands. The storm sewer invert at the subject lands is ~185.75m while the grade of the site at the southern limit is 185.25m – to extend storm sewer to the southern limit of the site the grade would have to be raised by approximately 2m. This would bring in a requirement for large retaining walls and significant fill import which would not be feasible.

Given the lack of available storm sewer at sufficient depth for the servicing of the site it was decided to maintain the existing drainage pattern, and provide on-site storage for stormwater in the form of low-impact development (LID) features which can provide both stormwater quality and quantity control.

A MIDUSS v2 simulation of the pre-development peak runoff rates was completed and the results are contained within Appendix 'D' for reference purposes. The Chicago 3-hour storm was used in this

analysis as it's peaked rainfall hyetograph presents a conservative analysis with high peak-flow rates. The table below summarizes the peak runoff rates to the southerly lands under the pre-development condition.

Return Period	2-Year	5-Year	100-Year
Area 1, Peak Flow (m <sup>3</sup> /s)	0.026	0.036	0.078

**Table 1: Pre-Development Drainage Peak Flow Rates**

MIDUSS v2 was then utilized to determine the amount of stormwater storage required in order to limit the post-development flows to the pre-development level for the 100-year return period 'worst-case' storm. Based on this analysis it was determined that 224 cubic meters of stormwater storage would be required.

The stormwater storage required will be provided through the use of permeable pavers in several areas of the development site. These areas are indicated on the post-development storm drainage area plan which is contained within Appendix 'D' for reference purposes. The permeable pavers are constructed on a base of 2" clear-stone which functions as a reservoir, capturing stormwater runoff and directing it to groundwater infiltration. Based on a 450mm clear stone reservoir, the permeable pavers will provide 0.18 cubic meters of stormwater storage per 1 square meter area. Based on the overall area of permeable pavers 285 cubic meters of storage is being provided on site within the paver reservoir.

In addition to the permeable pavers, a bio-swale is proposed to be provided at the site's southern limit. This bio-swale will further promote groundwater recharge and infiltration and based on it's proposed cross section it will provide a further 35 cubic meters of storage for stormwater runoff.

Given the proposed capture of stormwater through the permeable pavers and bioswale arrangement the peak runoff rates for the site under the post-development condition and the various return period storms is as follows:

Return Period	2-Year	5-Year	100-Year
Peak Runoff (m <sup>3</sup> /s, No SWM)	0.112	0.154	0.266
Storage Used (m <sup>3</sup> )	132.98	162.02	265.8
Peak Discharge (m <sup>3</sup> /s)	0.011	0.036	0.078

**Table 2: Post Development Drainage, Storage & Peak Flow Rates**

As can be seen, the proposed arrangement accounts for the required storage and will limit peak flows from the site to the pre-development level.

Given the expected clayey soil conditions the permeable pavers will be furnished with 100mm subdrain pipe outlets to convey stormwater to the adjacent swales and ultimately to the proposed bio-swale in the case that the underlying reservoir exceeds its maximum capacity.

Permeable pavers also provide a measure of stormwater quality control because stormwater contaminants are filtered by a filter cloth prior to entry to the reservoir, while smaller contaminants are passed through the sand filter located prior to re-entering the soil. The proposed bio-swale will also provide a measure of stormwater quality control as it also directs runoff to a sand filter prior to the ground water recharge. Under the proposed layout none of the stormwater runoff exiting the site is expected to carry sediment and thus the MECP stormwater criteria of 70% long term total suspended solids removal can be easily met and exceeded.

#### **2.4 Grading Considerations:**

As noted above, a topographic survey of the lot completed by The Larocque Group in 2022 is contained within Appendix 'A' for reference purposes. As can be seen there is a significant grade difference between the elevation of Garrison Road and the existing parking lot for the current building. From that parking area the site is relatively flat and drains southerly as noted in Section 2.3.

A preliminary Grading Plan has been provided within Appendix 'D' for reference and it illustrates how the site can be graded, with swales along both east and west property line draining from north to south, flat permeable paver areas and a flat bioswale with outlet to the lands to the south at the lowest area along the south property line. A final detailed Grading Plan can be provided for the site at the Site Plan stage.

### 3.0 Conclusion

In conclusion, based on the foregoing analysis we recommend that the proposal for the creation of the four new blocks on 1127 Garrison Road can be completed in accordance with the requirements of the Region of Niagara and Town of Fort Erie as follows:

1. Water servicing can be provided through a proposed 150mm watermain entering the site. Fire demands for the new dwellings will be 45 Lps based on the OBC Calculation for required fire-flows while peak domestic demand is expected to be 13.37 L/s. These water demands can be met through the local adjacent 300mm watermain on Garrison Road.
2. There is a proposed 200mm sanitary sewer on the property which can be used for the servicing of the new buildings. Based on a population of 270 persons for the 90 units a peak domestic sanitary flow rate of 3.52 L/s is expected to be generated from the site. The local 450mm trunk sanitary sewer on Garrison Road can accommodate this flow, while the local Alliston Avenue SPS can accommodate the domestic flows - but may not accommodate these flows based on local infiltration rates. Further discussion with the Region of Niagara should be carried out to determine if the single pump upgrade noted within the 2016 WWMSP will be required.
3. Drainage from the site cannot be directed to the Garrison Road storm sewers based on the grading constraints. It is proposed that a combination of permeable paver parking areas and bio-swale can be utilized to provide stormwater attenuation and limit peak runoff rates to the pre-development level while providing the appropriate level of stormwater quantity control.
4. A preliminary Grading Plan has been provided illustrating how the proposed development can be graded given the constraints of the local topography.

Thank you for your consideration of the above Functional Servicing Report should you have any questions or require clarification with respect to any part of the above please do not hesitate to contact the undersigned.

Respectfully submitted,



Andrew Smith, P. Eng.  
Principal & Director  
LandSmith Engineering & Consulting Ltd.



#### **4.0 Attachments:**

##### ***Appendix 'A'***

Concept Plan by Organica Studio + Inc.  
Topographic Survey by The Larocque Group

Preliminary Grading Plan  
Preliminary Servicing Plan

##### ***Appendix 'B'***

Fire Protection Plan  
Fire Flow Requirement Calculations – Unit 1, 2, 3  
Domestic Water Demand Calculations

##### ***Appendix 'C'***

Sanitary Drainage Area Plan  
Pages from Niagara Region Water / Wastewater Master Servicing Plan (2016)

##### ***Appendix 'D'***

Pre-Development Drainage Area Plan  
NPCA Figure re: Drainage Context  
Post-Development Drainage Area Plan  
Permeable Paver Fact Sheet  
Bio-Swale Fact Sheet

##### ***Appendix 'E'***

Garrison Road Plan & Profile, Sheet 6  
Garrison Road Plan & Profile, Sheet 7  
East Bertie Sewerage System Plan & Profile



**Attachments:**

Appendix 'A'

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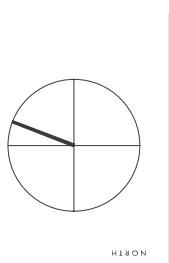
Concept Plan by Organica Studio + Inc.

Topographic Survey by The Larocque Group

Preliminary Grading Plan

Preliminary Servicing Plan

CONCEPTUAL SITE PLAN AND DESIGN TO BE REVIEWED BY THE CHIEF ENGINEER OF THE DISTRICT OF COLUMBIA. THIS PLAN IS A PRELIMINARY DESIGN AND IS NOT TO BE USED FOR CONSTRUCTION. THE CHIEF ENGINEER OF THE DISTRICT OF COLUMBIA IS NOT RESPONSIBLE FOR THE ACCURACY OF THIS PLAN. THE CHIEF ENGINEER OF THE DISTRICT OF COLUMBIA IS NOT RESPONSIBLE FOR THE ACCURACY OF THIS PLAN. THE CHIEF ENGINEER OF THE DISTRICT OF COLUMBIA IS NOT RESPONSIBLE FOR THE ACCURACY OF THIS PLAN.



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2	REVISION FOR PLAN FOR COORDINATION	2023/09/19

1127 GARRISON ROAD, FORT ERIE

## STACKED DWELLINGS

### SITE PLAN

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[Symbol]	EXISTING/PROPOSED WOOD FENCE
[Symbol]	PROPOSED RETAINING WALL

**CONCEPTUAL SITE STATISTICS**

LOT AREA	10,047.03 SQ. M. (1,00 HECTARES)
C3 ZONE AREA	3,443.25 SQ. M.
IMP. ZONE AREA	6,604.68 SQ. M.
LOT COVERAGE	18.25%
LANDSCAPING IN C3 ZONE	3,102.92 SQ. M.
BUILDING HEIGHT	12.2M (ALL BLOCKS)
PROPOSED UNIT TYPES	90 DWELLING UNITS
PROPOSED DENSITY	9.0 UNITS/HECTARE
PROPOSED PARKING	119 BICYCLE PARKING SPACES, 12 COMMERCIAL SPACES, 6 TYPE A ACCESSIBLE SPACES, 6 TYPE B ACCESSIBLE SPACES

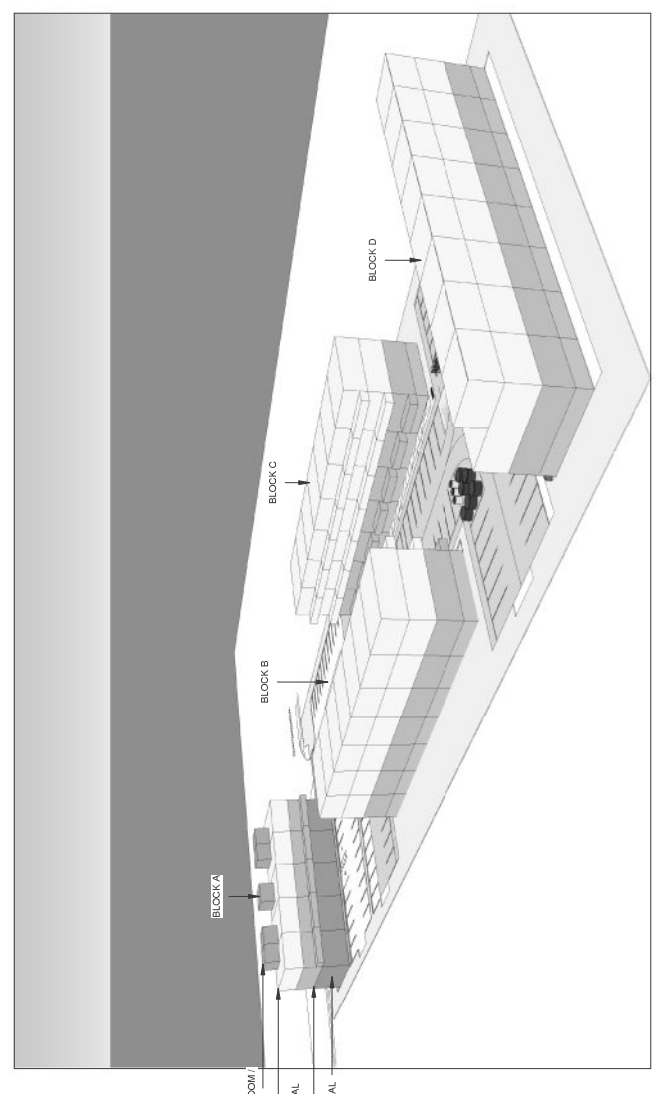
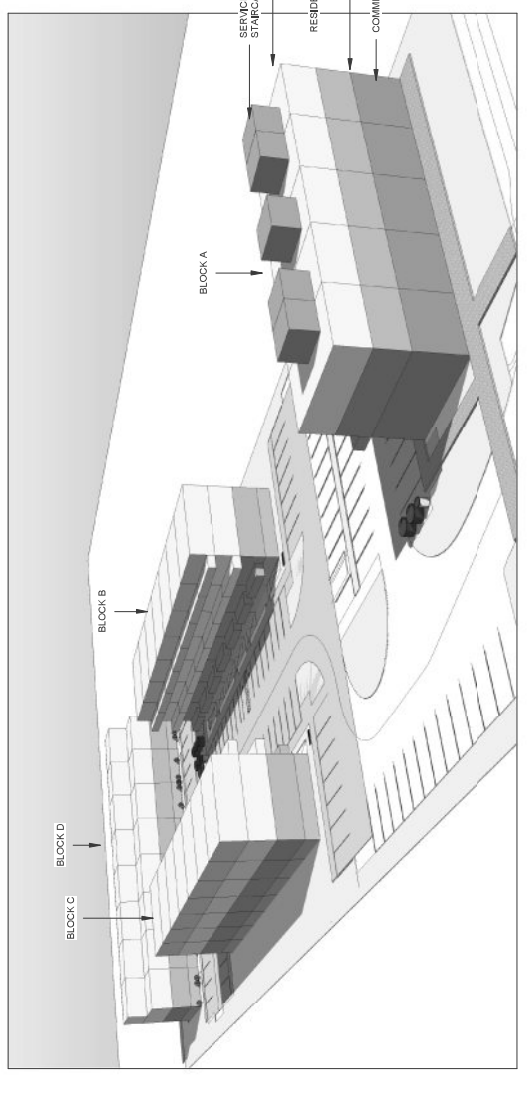
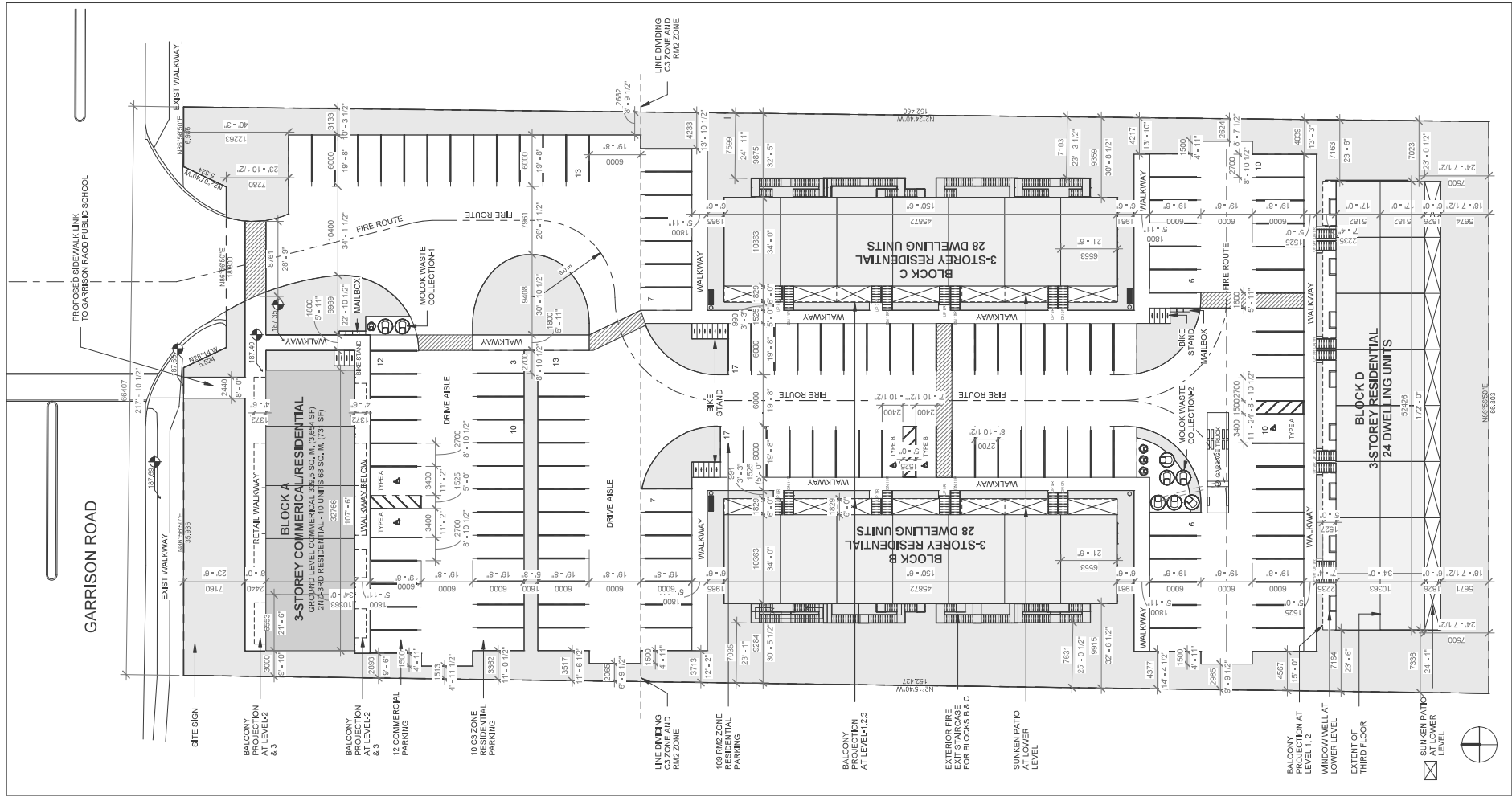
**AREA SCHEDULE (GROSS BUILDING)**

BLOCK	METRIC AREA	IMPERIAL AREA
A (RESIDENTIAL)	679 m <sup>2</sup>	7298.7 ft <sup>2</sup>
A (COMMERCIAL)	335.5 m <sup>2</sup>	3,624 ft <sup>2</sup>
B	1,901.5 m <sup>2</sup>	20,468 ft <sup>2</sup>
C	1,901.5 m <sup>2</sup>	20,468 ft <sup>2</sup>
D	1,901.5 m <sup>2</sup>	20,468 ft <sup>2</sup>
<b>TOTAL</b>	<b>6,723 m<sup>2</sup></b>	<b>72,862.7 ft<sup>2</sup></b>

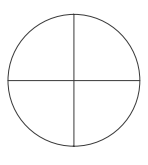
  

**CONCEPTUAL UNIT AREAS**

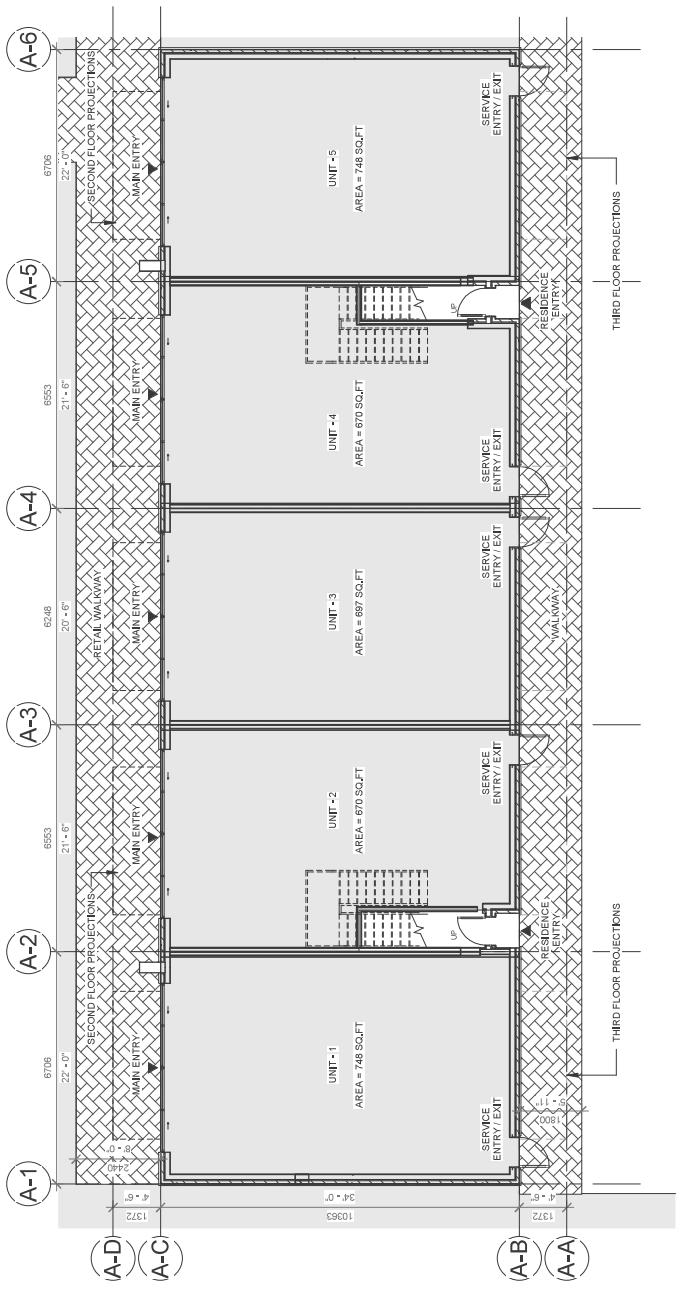
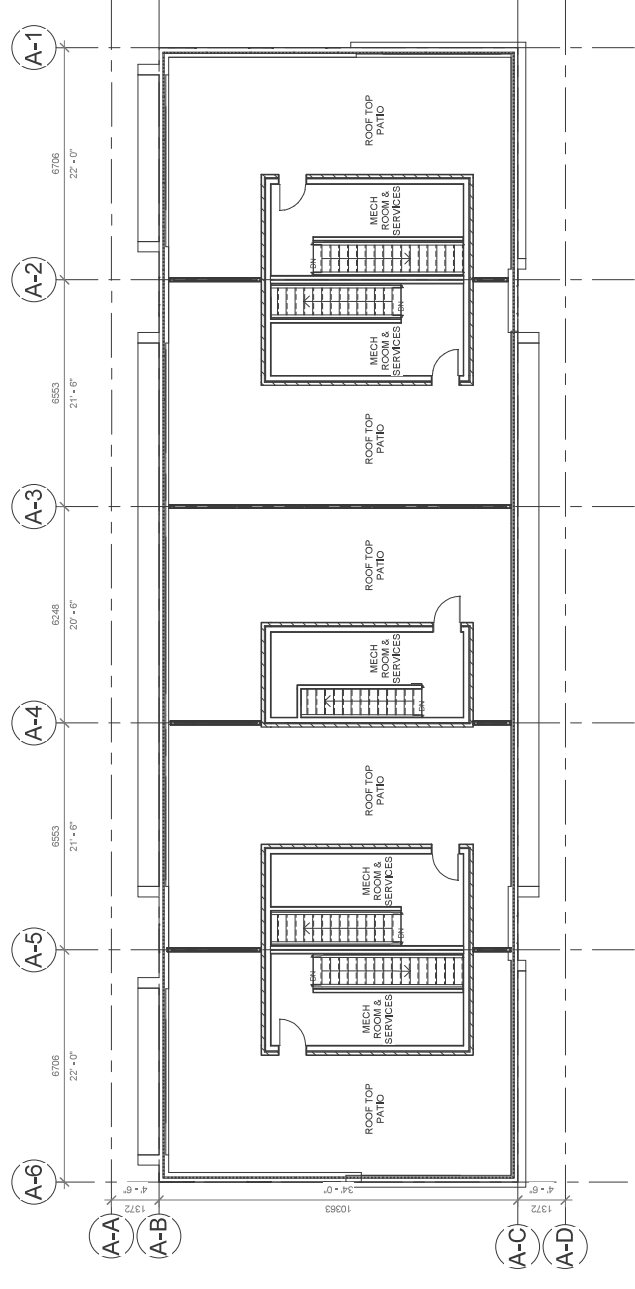
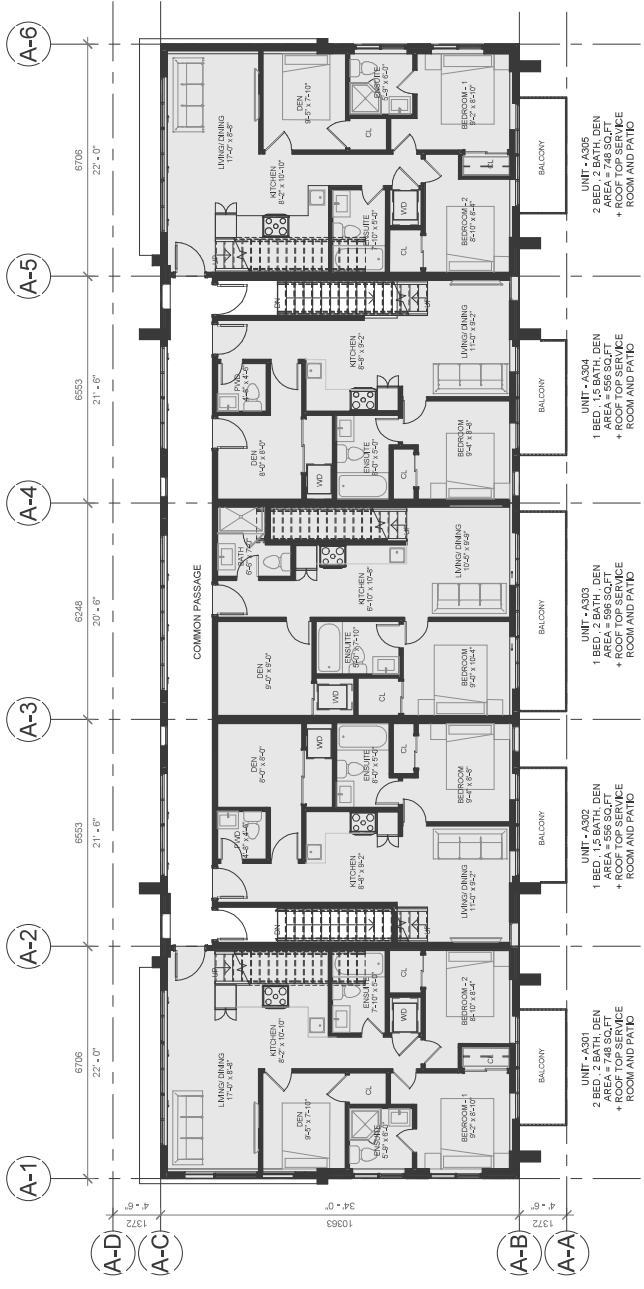
3 BEDROOM UNITS	MIN. AREA = 79 SQ. M.
2 BEDROOM UNITS	MIN. AREA = 60 SQ. M.
1 BEDROOM UNITS	MIN. AREA = 50 SQ. M.



Contractor shall design and detail as shown on the drawings. The design and all associated documents are an extension of any drawings, specifications, and all associated documents prepared by the architect. The contractor shall be responsible for obtaining all necessary permits and approvals from the relevant authorities. The contractor shall be responsible for obtaining all necessary permits and approvals from the relevant authorities. The contractor shall be responsible for obtaining all necessary permits and approvals from the relevant authorities.



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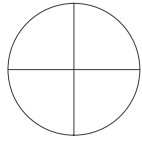
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Consulting, design and design services are provided by the Designer. The Designer shall retain and deliver to the Client the original design files, including all digital files and source files in all formats and all associated documents and information in all formats. The Client shall retain and deliver to the Designer all information, including all digital files and source files in all formats and all associated documents and information in all formats. The Designer shall not be responsible for any information, including all digital files and source files in all formats and all associated documents and information in all formats, that is not provided by the Client. The Designer shall not be responsible for any information, including all digital files and source files in all formats and all associated documents and information in all formats, that is not provided by the Client. The Designer shall not be responsible for any information, including all digital files and source files in all formats and all associated documents and information in all formats, that is not provided by the Client.



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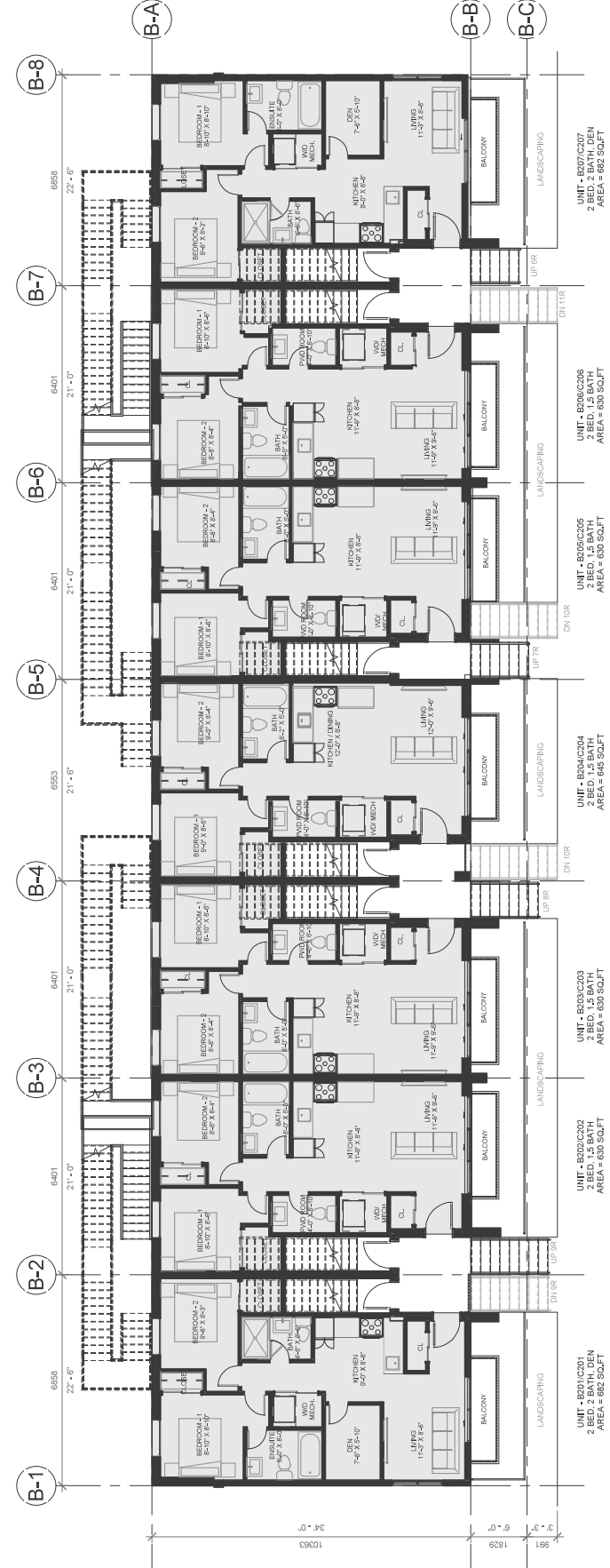
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 1177 GARRISON ROAD, FORT ERIE

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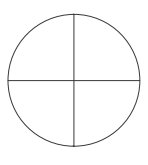


① Block B & C - Lower Level  
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② Block B & C - Ground Level  
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Consulting, design, and construction services provided by Organic Studio + Inc. are subject to the terms and conditions of the Organic Studio + Inc. Standard Contract Documents, which are available at [www.organicstudio.com](http://www.organicstudio.com). The design of this project is the property of Organic Studio + Inc. and shall remain the property of Organic Studio + Inc. until such time as the client has accepted the final design documents. The client shall be responsible for obtaining all necessary permits and approvals from the appropriate authorities. The client shall be responsible for providing all necessary information and data to Organic Studio + Inc. in a timely manner. Organic Studio + Inc. shall not be held responsible for any errors or omissions in the design documents, or for any consequences arising from the use of the design documents. The client shall be responsible for obtaining all necessary permits and approvals from the appropriate authorities. The client shall be responsible for providing all necessary information and data to Organic Studio + Inc. in a timely manner. Organic Studio + Inc. shall not be held responsible for any errors or omissions in the design documents, or for any consequences arising from the use of the design documents.



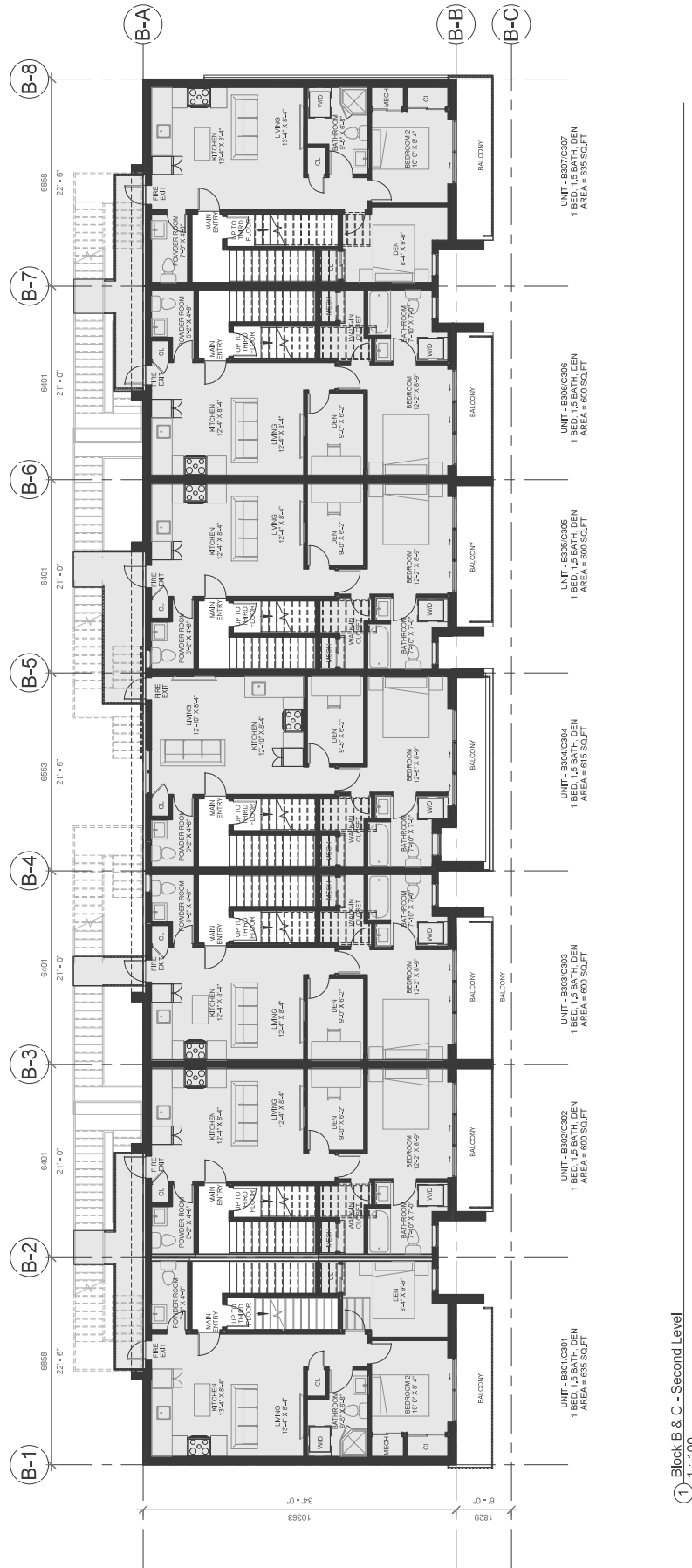
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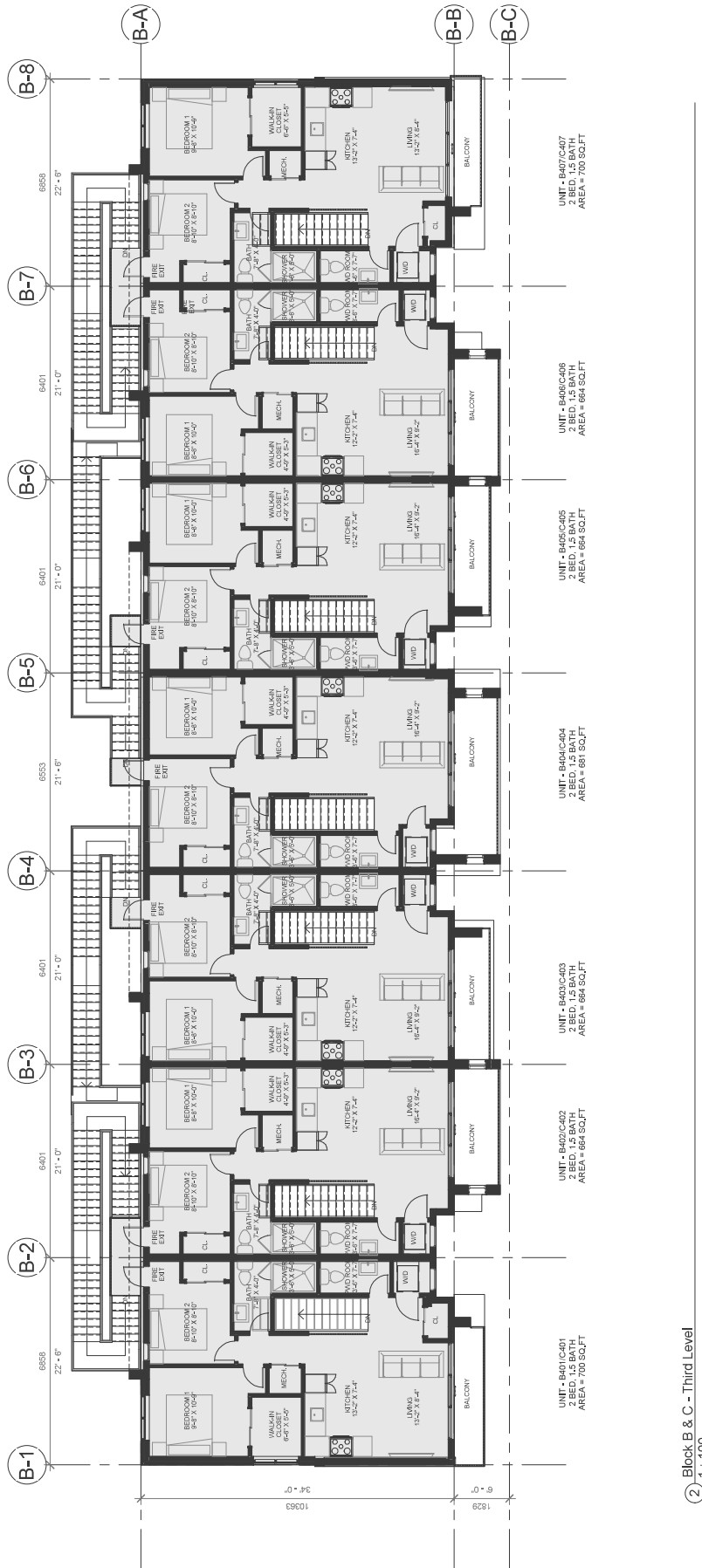
BLOCKS B & C - FLOOR PLANS  
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 1177 GARRISON ROAD, FORT ERIE

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② Block B & C - Third Level  
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# BLOCKS D - FLOOR PLANS

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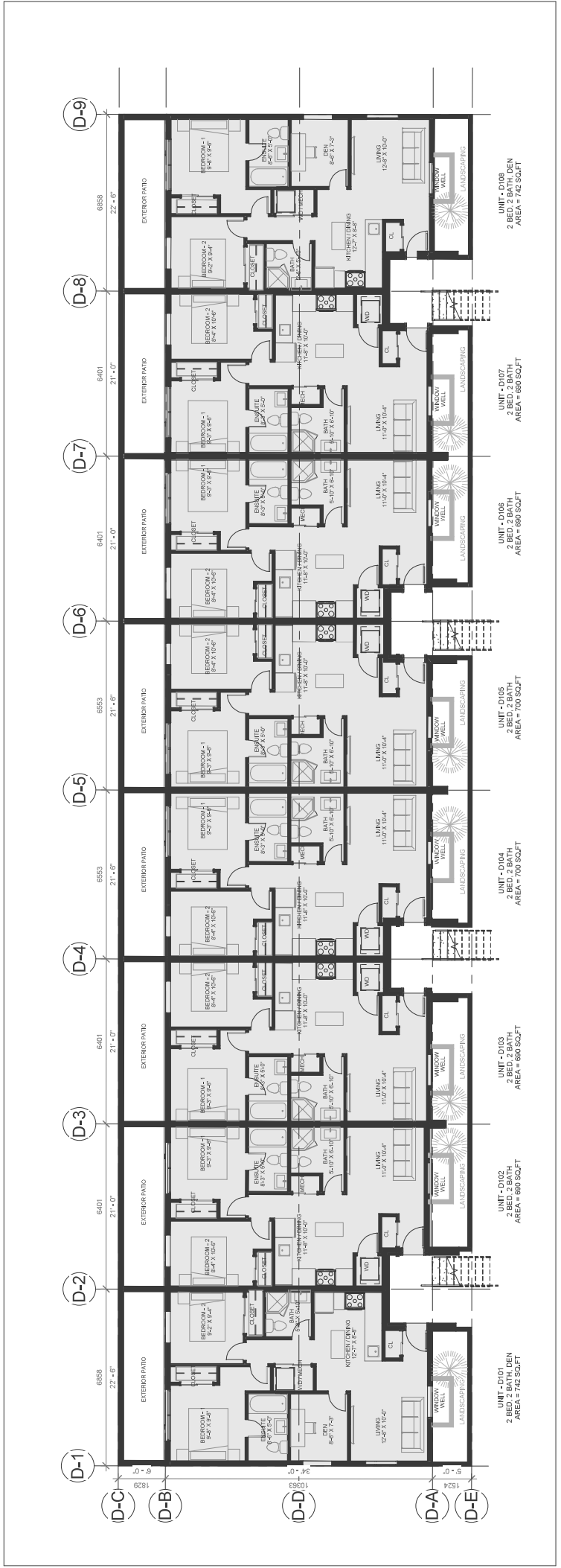
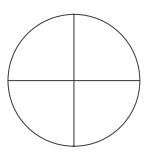
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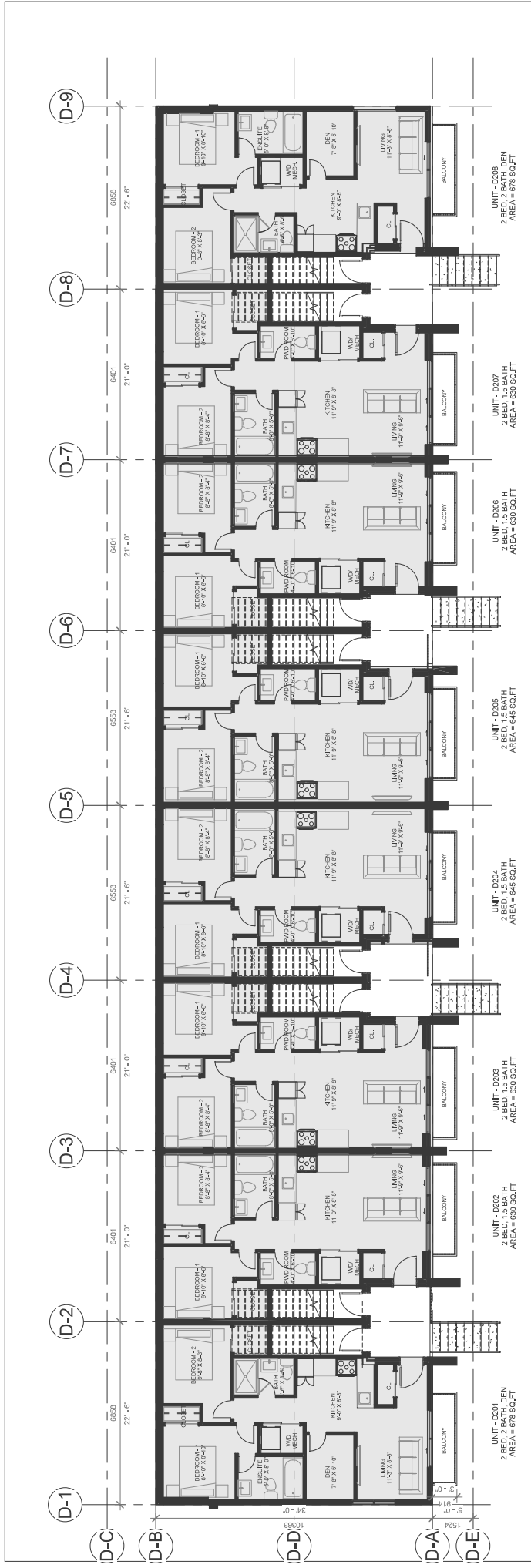
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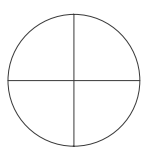


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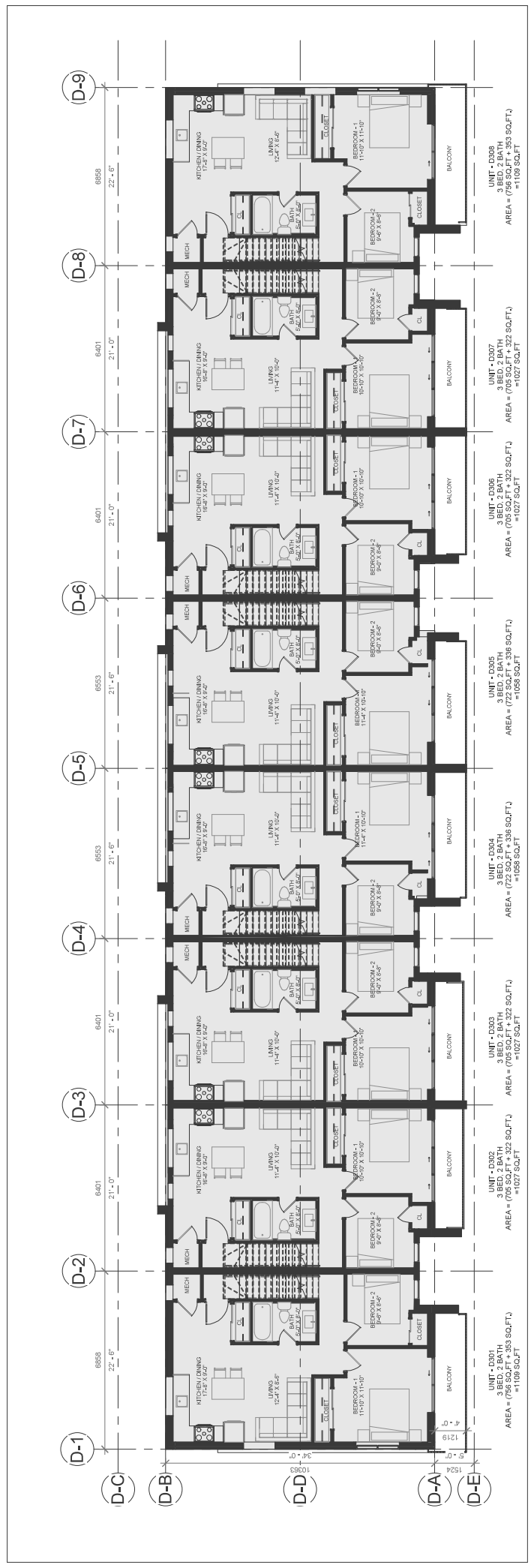


② Block D - Ground Level  
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Consultant's design and design team shall retain the copyright in all architectural drawings, designs, concepts, and data created by them, and shall be responsible for the coordination of all drawings and designs. The design team shall not be responsible for the coordination of drawings and designs created by third parties. The design team shall be responsible for the coordination of drawings and designs created by third parties. The design team shall be responsible for the coordination of drawings and designs created by third parties.

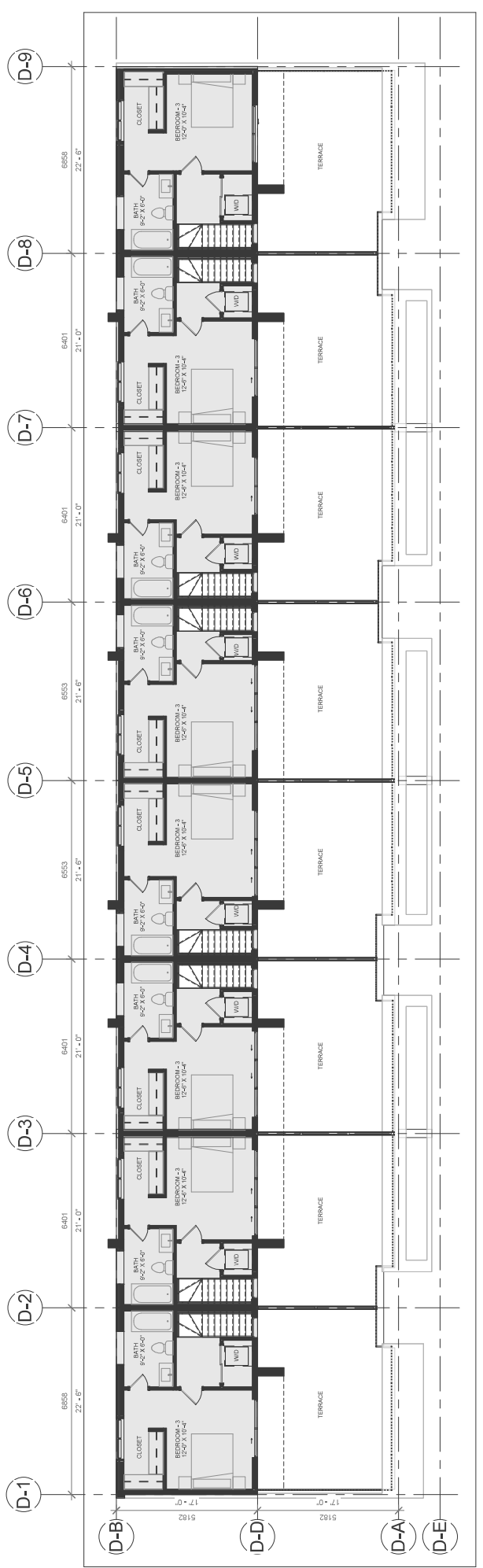


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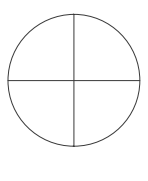
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1177 GARRISON ROAD, FORT ERIE

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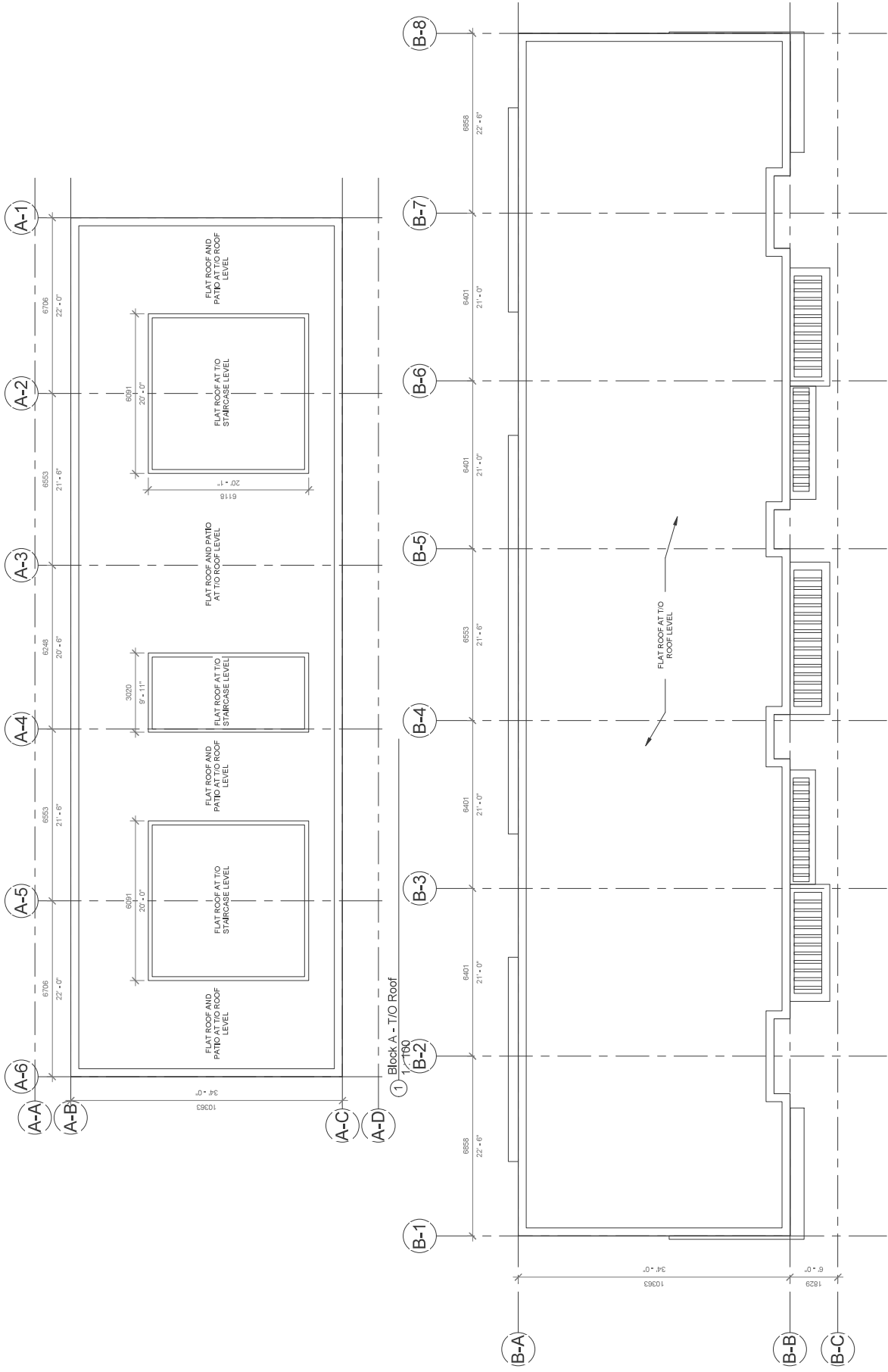


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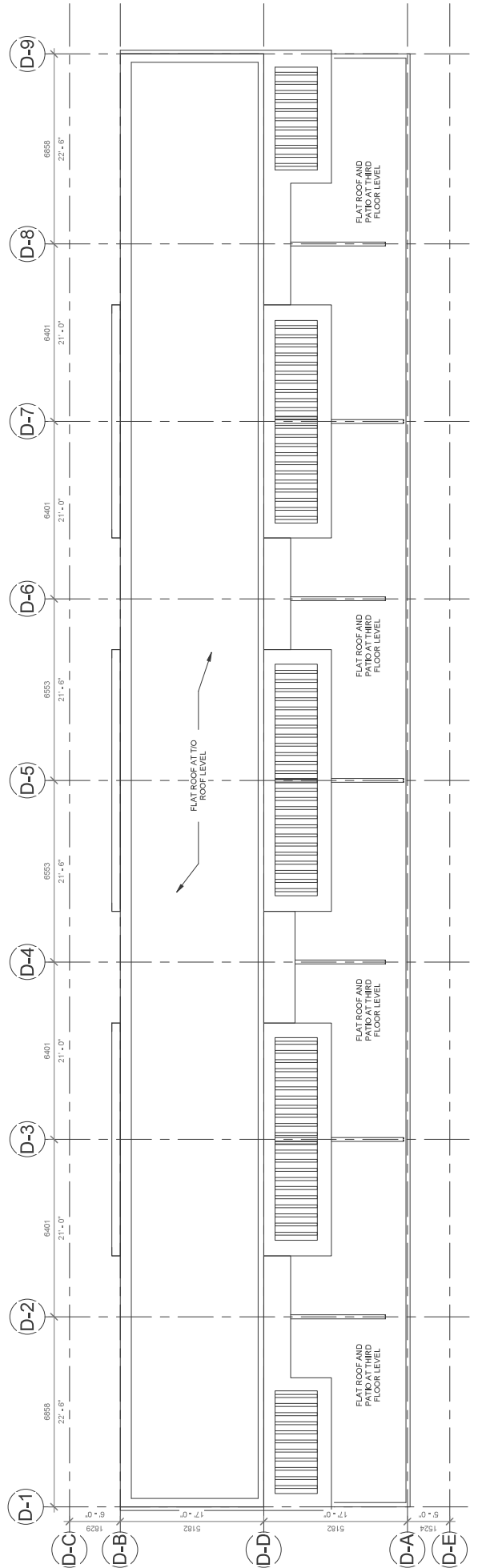
NO.	DESCRIPTION	DATE
1	ISSUED FOR PERMITS	2023.09.19

ROOF PLANS  
 STACKED DWELLINGS

SCALE: 1/160  
 DATE: 2023-09-19 10:59 AM  
 DRAWN: Author  
 CHECKED: Checker  
 PROJECT NUMBER: 21084  
 SHEET



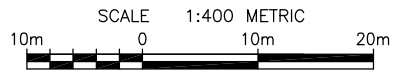
3 Block B & C - Roof Level  
 1 : 100



4 Block D - Roof Level  
 1 : 100



SITE CONDITION PLAN  
**PART OF LOT 4**  
**CONCESSION 3 LAKE ERIE**  
 (GEOGRAPHIC TOWNSHIP OF BERTIE)  
**TOWN OF FORT ERIE**  
 REGIONAL MUNICIPALITY OF NIAGARA



**REGIONAL ROAD No. 3**

(BY BY-LAW No. 8954-98, TRANSFERRED BY ORDER-IN-COUNCIL  
 O.C. 540/97, DESCRIBED IN INSTRUMENT No. 724387 AND LT116209)

**GARRISON ROAD**

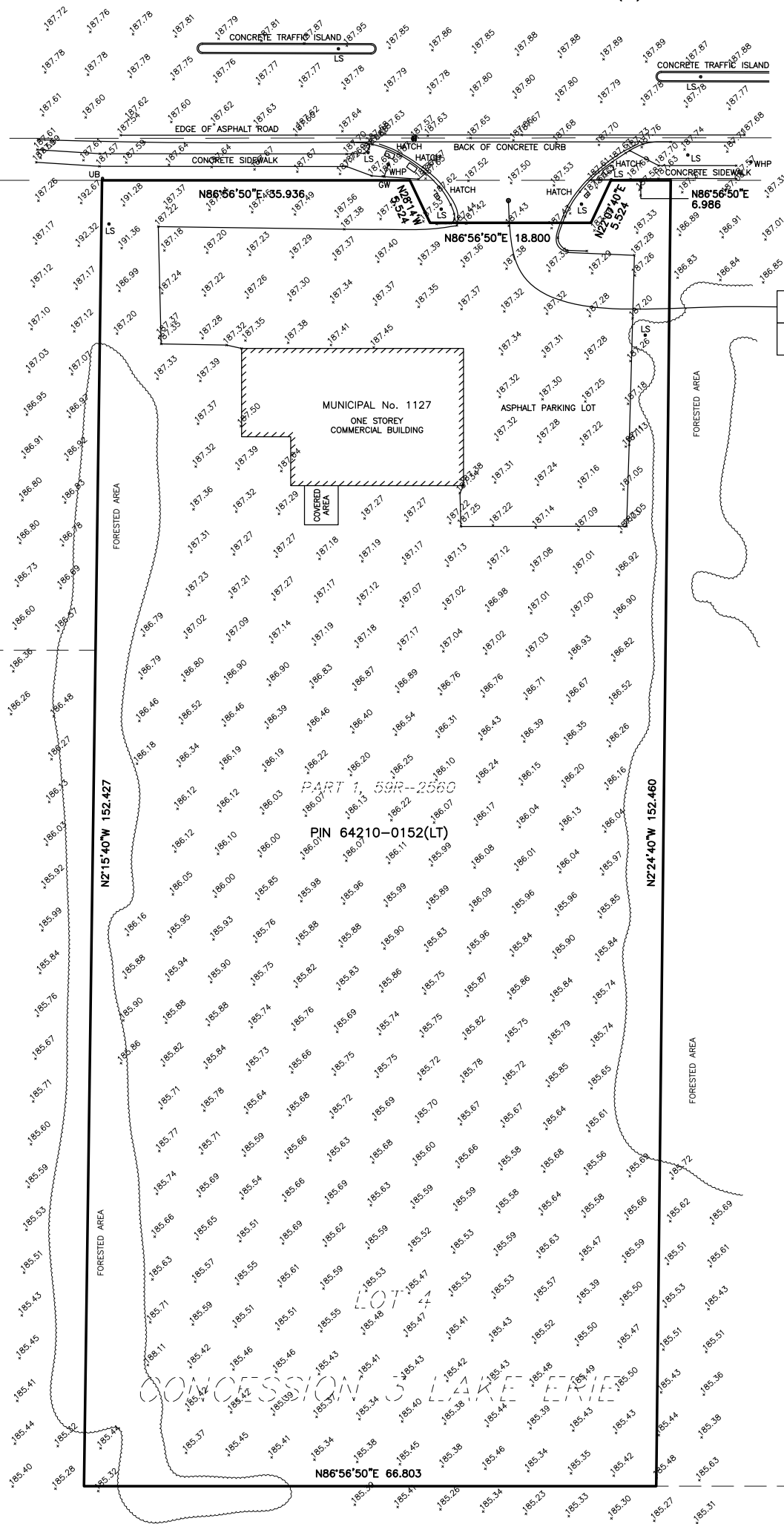
(AS LOCALLY KNOWN)  
 (ORIGINAL ROAD ALLOWANCE BETWEEN CONCESSION 3  
 LAKE ERIE AND CONCESSION 4 NIAGARA RIVER)  
 PIN 64236-0425(LT)



WIDENED BY EXPROPRIATION PLAN No. BB4584

PIN 64210-0154(LT)

PART 2, 59R-11500



PART 2, 59R-11336  
 PIN 64210-0151(LT)

PIN 64210-0065(LT)  
 PART 2, 59R-2560

**LEGEND**

- CB DENOTES CATCH BASIN
- GW DENOTES GUY WIRE
- LS DENOTES LIGHT STANDARD
- UB DENOTES UTILITY BOX
- WHP DENOTES WOOD HYDRO POLE
- 188.20 DENOTES EXISTING ELEVATION

**BEARING NOTE**

BEARINGS HEREON ARE GRID BEARINGS PREVIOUSLY ESTABLISHED BY THE LAROCQUE GROUP AND ARE REFERRED TO THE CENTRAL MERIDIAN 81°00'W LONGITUDE, ZONE 17, UNIVERSAL TRANSVERSE MERCATOR (6° UTM). THESE VALUES ARE NAD83 (CSRS v7) EPOCH 2010.0 REFERENCE SYSTEM.

**ELEVATION NOTE**

ELEVATIONS HEREON ARE ORTHOMETRIC AND ARE RELATED TO CGVD28, HT2, AS PREVIOUSLY ESTABLISHED BY THE LAROCQUE GROUP.

**METRIC NOTE**

DISTANCES AND CO-ORDINATES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048.

DISTANCES SHOWN ON THIS PLAN ARE ADJUSTED GROUND LEVEL DISTANCES AND CAN BE USED TO COMPUTE GRID CO-ORDINATES BY MULTIPLYING THE DISTANCES BY A COMBINED SCALE FACTOR OF 0.99991850.



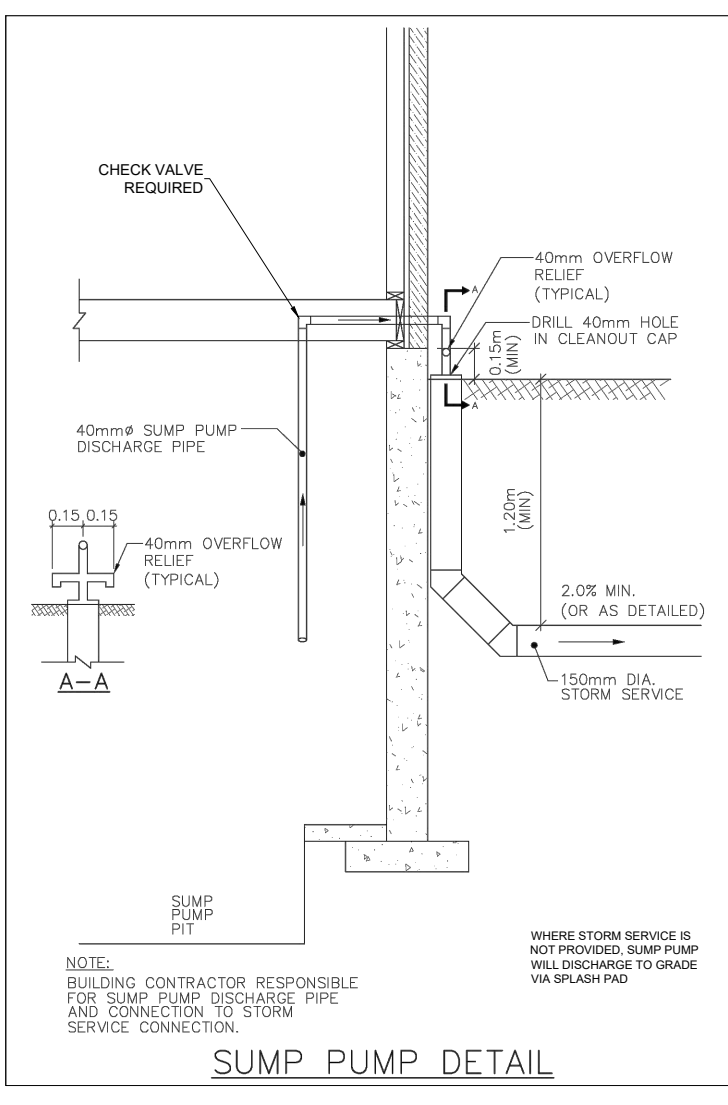
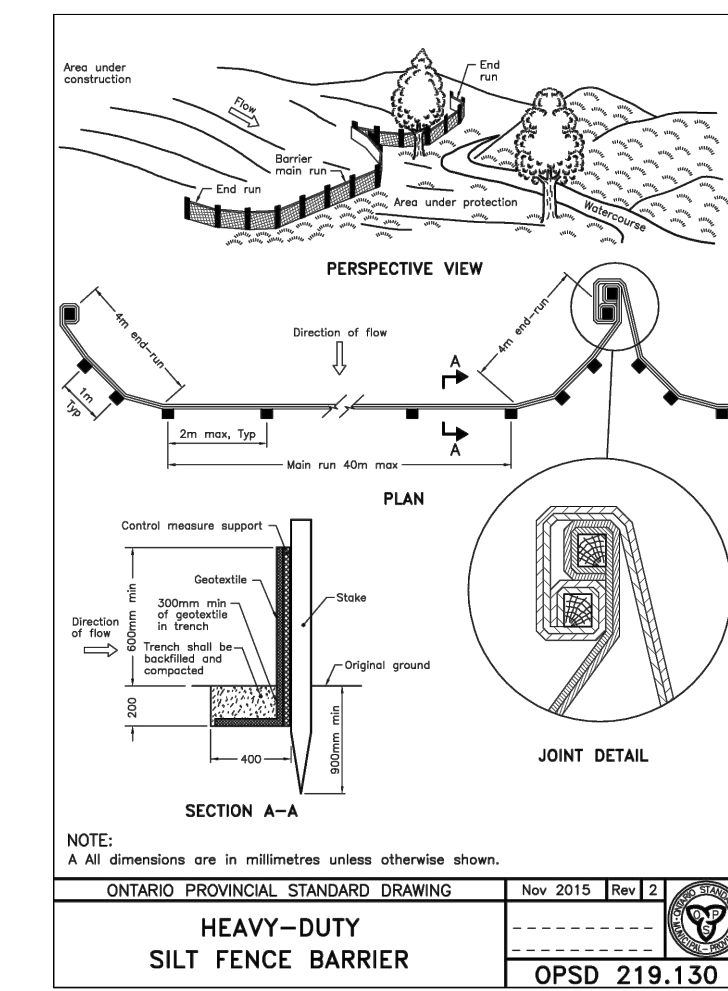
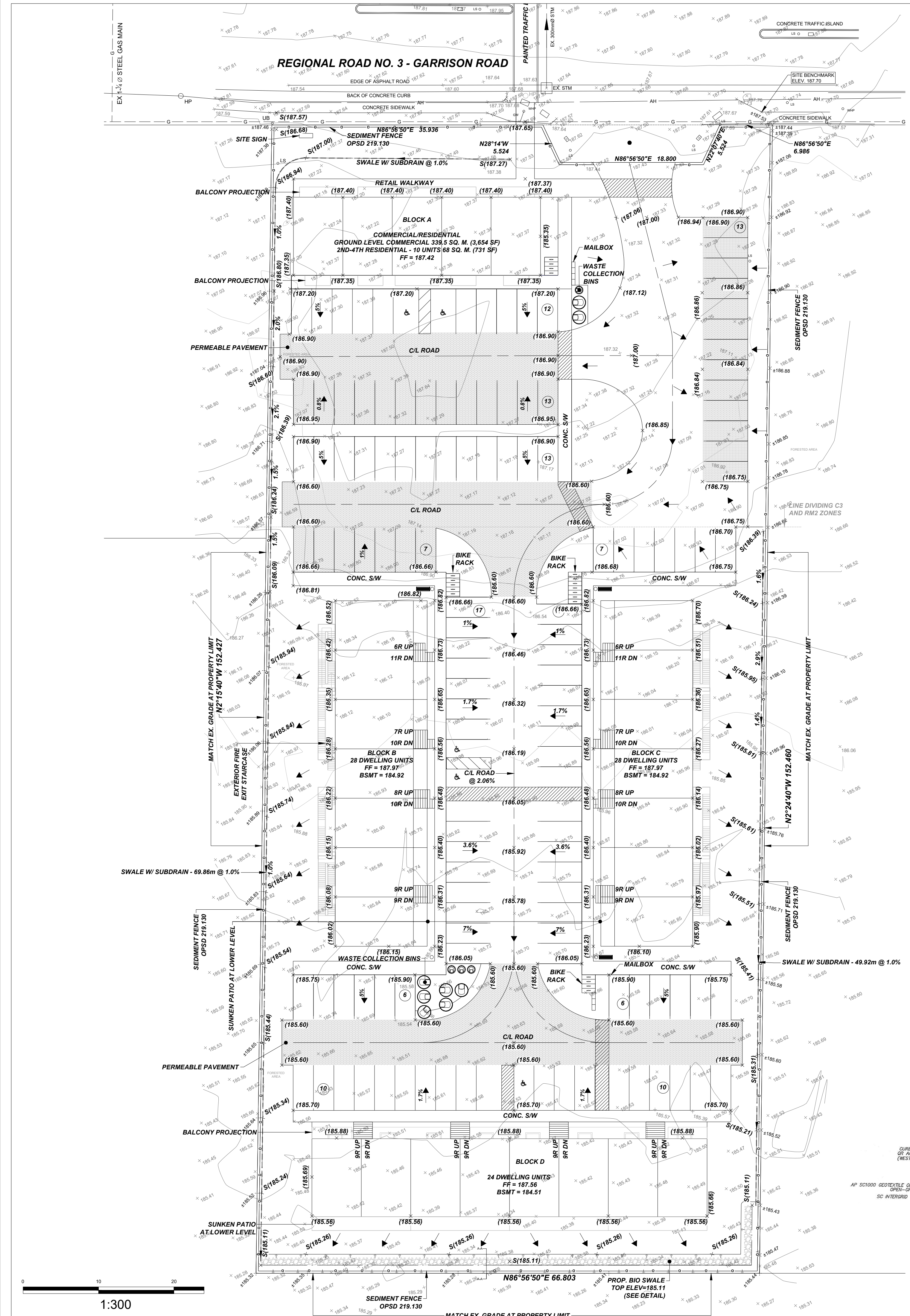
**THE LAROCQUE GROUP**

O.L.S./PROJECT CONSULTANTS/LAND MANAGEMENT  
 12 LYMAN STREET, ST. CATHARINES, ONTARIO  
 905-688-1413  
 6385 COLBORNE STREET, NIAGARA FALLS, ONTARIO  
 905-358-8400  
 www.larocquegroup.ca

PIN 64210-0061(LT)

PART 2, 59R-1298

DATE : SEPTEMBER 20, 2022 FILE No. : NS2022-048  
 DWG.FILE : NS2022-048-01



**LEGEND**

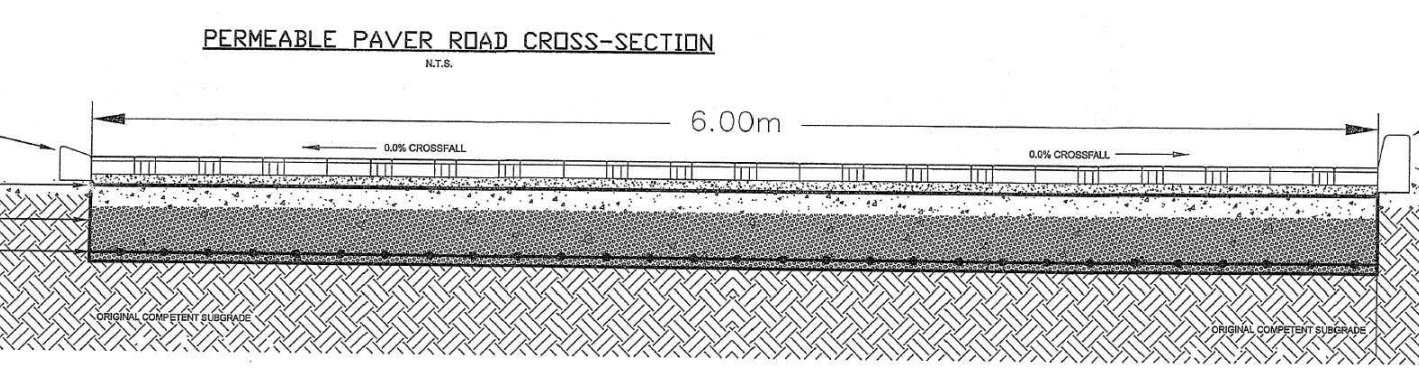
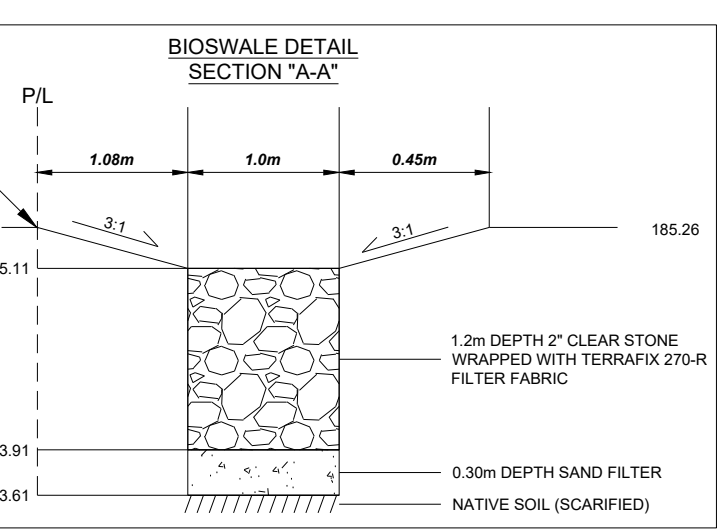
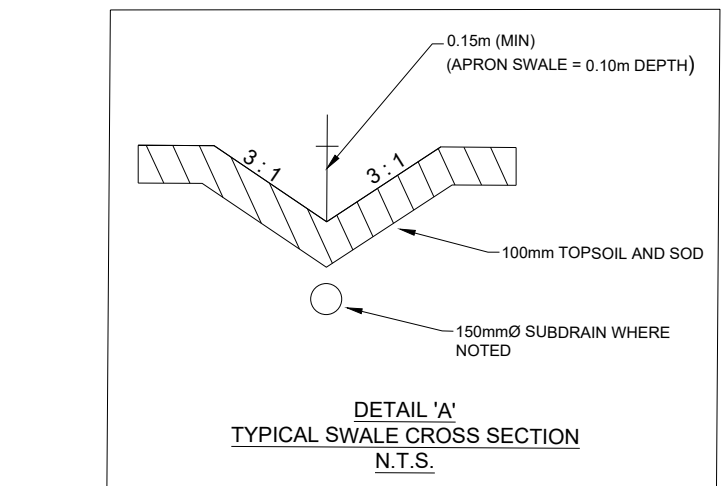
- Existing Elevation
- Existing Elevation (Calculated)
- Proposed Elevation
- Proposed Apron Elevation
- Proposed Swale Elevation
- Proposed Downspout
- Proposed Entrance Location
- Proposed Swale
- Proposed Swale with Subdrain
- Proposed Silt Fence
- Proposed Permeable Pavement

**GENERAL GRADING NOTES:**

- MATCH EXISTING GRADE AT PROPERTY / DEVELOPMENT LIMITS WITH SLOPED SIDES OF MAXIMUM 3:1 AND/OR RETAINING WALLS AS SPECIFIED.
- SLOPES OF SWALES FOR BOTH "BACK-TO-FRONT" AND "SPLIT" DRAINAGE SHALL BE NO LESS THAN 2.0% AND NO GREATER THAN 5.3% (3:1).
- MINIMUM GRADE FOR APRON "WRAP-AROUND" SWALE AT THE REAR OF THE UNIT SHALL BE 1.0%.
- WHEN MATCHING TO EXISTING GRADE AT THE LIMITS OF THE DEVELOPMENT / PROPERTY WHERE 2.0% SLOPE CANNOT BE REASONABLY ACHIEVED A 1.5% GRADE IS PERMITTED PROVIDED A 150MM SUB-DRAIN IS INSTALLED WITH THE SWALE AS PER RD-121 AND CONNECTED TO A SUITABLE OUTLET.
- DRIVEWAY SLOPES SHALL NOT BE LESS THAN 2.0% AND SHALL NOT BE MORE THAN 7.0%. REVERSED SLOPED DRIVEWAYS ARE NOT ALLOWED FOR ANY NEW CONSTRUCTION.
- GARAGE FLOOR ELEVATION SHALL BE SET A MINIMUM OF 0.30M HIGHER THAN THE BACK OF WALK, UNLESS OTHERWISE SPECIFIED.
- THE TOP OF FOUNDATION WALL FOR THE DWELLING UNIT SHALL BE A MINIMUM 150MM (6") ABOVE FINISHED GRADE.
- UNLESS OTHERWISE NOTED, THE GROUND BETWEEN PROPOSED ELEVATIONS SHALL BE GRADED AS A STRAIGHT LINE.
- IF GRADING IS REQUIRED ON LANDS ADJACENT TO THE PROPERTY / DEVELOPMENT WHICH ARE NOT OWNED BY THE DEVELOPER, THEN THE DEVELOPER MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNER, OTHERWISE RETAINING WALLS MUST BE USED.
- ALL RETAINING WALLS SHALL BE PLACED A MINIMUM 0.45M FROM PROPERTY LINES.
- ANY WALL OF GREATER HEIGHT THAN 1.0M MUST BE DESIGNED BY A PROFESSIONAL ENGINEER.
- TOP OF RETAINING WALL ELEVATIONS SHALL BE SET A MINIMUM OF 150MM ABOVE THE PROPOSED SIDE-YARD SWALES.
- RETAINING WALLS 0.60M AND HIGHER REQUIRE CONSTRUCTION OF A FENCE OR GUARD RAIL AT THE TOP OF THE REAR OF THE WALL. SUCH FENCES OR GUARD RAILS SHALL BE DESIGNED AND CONSTRUCTED IN ACCORDANCE WITH THE REQUIREMENTS OF THE ONTARIO BUILDING CODE.
- ALL FILL COMPACTED ON THE LOT(S) SHALL BE COMPACTED TO A MINIMUM 95% SPD (UNLESS OTHERWISE RECOMMENDED BY A GEOTECHNICAL ENGINEER). MATERIALS SHALL BE PLACED IN LIFTS NOT EXCEEDING 300MM DEPTH.
- FOR DELINEATION OF TREE PROTECTION ZONES, BUFFERS, REMOVALS, AND PROTECTION SCHEMATICS REFER TO THE TREE PROTECTION PLAN (IF APPLICABLE).

**BACKYARD GRADING NOTES:**

- "REQUIRED BACKYARD" SHALL BE A MINIMUM OF 6.0 METRES UNLESS OTHERWISE DEFINED IN THE APPLICABLE ZONING BY-LAW.
- THE MAXIMUM SLOPE IN THE BACKYARD ADJACENT TO THE BUILDING FOR A DISTANCE EQUAL TO THE REQUIRED BACKYARD SHALL BE 5% EXCEPT FOR SIDE OR REAR YARD SWALES AND RETAINING WALLS.
- WHERE THE 5% RESTRICTION ON THE BACKYARD'S GRADES RESULTS IN ELEVATION DIFFERENCES BETWEEN ADJACENT PROPERTIES, RETAINING WALL SHALL BE CONSTRUCTED ALONG THE SIDES AND BACK OF THE LOT.
- GENERALLY, SLOPES SHALL BE PLACED ON THE LOWER LOT, WHEREAS RETAINING WALLS SHALL BE PLACED ON THE HIGHER LANDS.
- THE 5% RESTRICTION DOES NOT PRECLUDE RETAINING WALLS IN THE REQUIRED BACKYARDS PROVIDING THE TERRACES ARE MAINTAINED TO THE 5% GRADE AS SET OUT ABOVE. THE INTENTION OF THIS PROVISION IS TO PROVIDE FLEXIBILITY OF HOUSE CONSTRUCTION.
- BACK TO FRONT DRAINAGE SHALL ONLY BE PERMITTED WHERE THE COMBINED SIDE YARD SETBACK IS 2.0M OR MORE. PROVIDING A MINIMUM OF 2.0M BETWEEN FOUNDATION WALLS FOR DRAINAGE SWALES. A 1.2M SETBACK IS REQUIRED ON THE GARAGE SIDE OF THE LOT.



**NOTES:**

- LOCATIONS UNDERGROUND SERVICES ARE APPROXIMATE AND MUST BE FIELD VERIFIED PRIOR TO CONSTRUCTION.
- ANY DISCREPANCIES BETWEEN SERVICE LOCATIONS AND THESE ENGINEERING DRAWINGS MUST BE BROUGHT TO THE ATTENTION OF THE PROJECT ENGINEER.
- THIS PLAN SHALL BE INTERPRETED IN CONJUNCTION WITH THE SITE PLAN DRAWING PREPARED BY CUSTOMER ARCHITECT (LATEST VERSION). ANY DISCREPANCIES MUST BE BROUGHT TO THE ENGINEER'S ATTENTION IMMEDIATELY.



**KEY PLAN N.T.S.**

**BENCHMARK NOTE:**  
ELEVATIONS HEREON ARE ORTHOMETRIC AND ARE RELATED TO CGVD28, HT2, AS PER THE LAROQUE GROUP.

**SITE BENCHMARK:**  
CONCRETE SIDEWALK CORNER, NORTH-EAST OF 1127 GARRISON ROAD.  
ELEVATION = 187.70m

**GENERAL NOTES:**

- TENDERER SHALL SATISFY THEMSELVES AS TO THE NATURE OF THE GROUND AND BID ACCORDINGLY.
- ALL ROCK LINE INDICATIONS SHOWN ON THE PLAN MUST BE VERIFIED BY THE CONTRACTOR.
- CONTRACTOR SHALL VERIFY LOCATIONS AND INVERTS OF ALL EXISTING SANITARY AND STORM SEWERS AND WATERMANS. PRIVATE DRAINS AND WATER SERVICES, GAS MAINS, CABLE TV, HYDRO AND TELEPHONE DUCTS ETC AT START OF CONSTRUCTION.

NO.	DATE:	DESCRIPTION:
3	2023-09-15	ISSUED WITH FSR
2	2023-09-15	ISSUED WITH FSR
1	2023-09-05	ISSUED FOR CLIENT REVIEW
0	2023-03-14	ISSUED FOR FSR

**REVISIONS**

SEAL

**CLIENT:**  
TRINITYSTAR AQUILA INC.

**MUNICIPALITY:**  
TOWN OF FORT ERIE

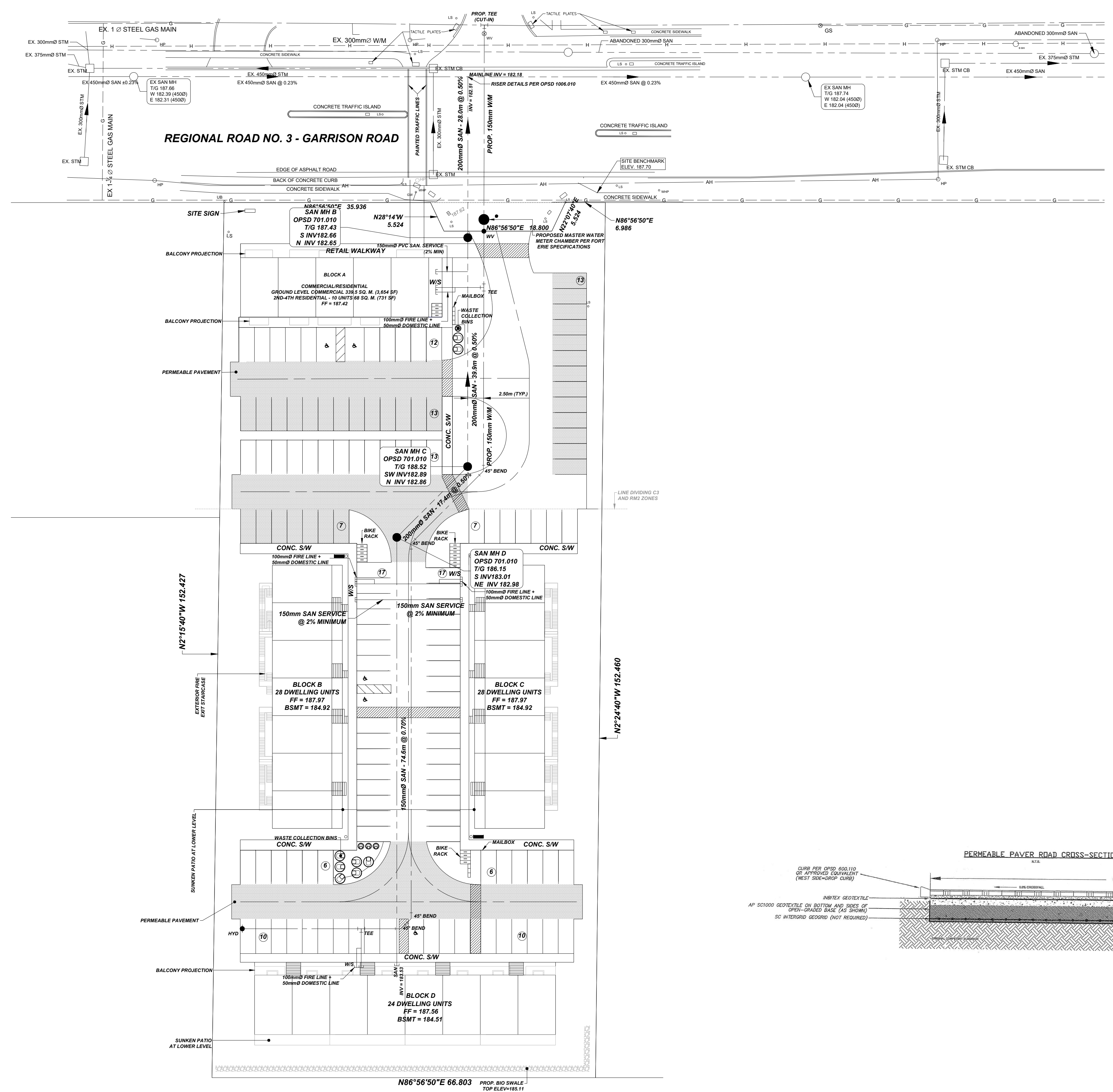
**PROJECT NAME:**  
1127 GARRISON RD.

**TITLE:**  
GRADING PLAN

**SCALE:** 1:300  
**DATE:** 2022-12-13

**CHECKED BY:** AS  
**DESIGNED BY:** AS

**DWG No:** 22038TSA  
**SHEET No:** 1



### LEGEND

○ LS	EXISTING LIGHT STANDARD	_____	EXISTING AERIAL HYDRO
● WV	PROPOSED WATER VALVE	_____	EXISTING WATERMAIN
TEE	PROPOSED WATERMAIN TEE	_____	PROPOSED WATER SERVICE
□ PLUG	PROPOSED PLUG	_____	EXISTING SANITARY
● CS	PROPOSED CURB STOP	_____	PROPOSED SANITARY
○ WV	EXISTING WATER VALVE	_____	EXISTING STORM
○ GM	EXISTING GAS METER	_____	PROPOSED STORM
○ HP	EXISTING HYDRO POLE		
□ CB	EXISTING CATCH BASIN		
○ SAN	EXISTING SANITARY MAINTENANCE HOLE		
● SAN	PROPOSED SANITARY MAINTENANCE HOLE		
□ PLUG	EXISTING PLUG		
□ PLUG	PROPOSED PLUG		
○ STM MH	EXISTING STORM MAINTENANCE HOLE		
● STM MH	PROPOSED STORM MAINTENANCE HOLE		
□ CB	EXISTING CATCH BASIN		
■ CB	PROPOSED CATCH BASIN		
□ DCB	EXISTING DOUBLE CATCH BASIN		
■ DCB	PROPOSED DOUBLE CATCH BASIN		
● HYD	PROPOSED FIRE HYDRANT		
● FH	EXISTING FIRE HYDRANT		



**KEY PLAN** N.T.S.

**BENCHMARK NOTE:**  
ELEVATIONS HEREON ARE ORTHOMETRIC AND ARE RELATED TO CGVD28, HT2, AS PER THE LAROQUE GROUP.

**SITE BENCHMARK:**  
CONCRETE SIDEWALK CORNER, NORTH-EAST OF 1127 GARRISON ROAD.  
ELEVATION = 187.70

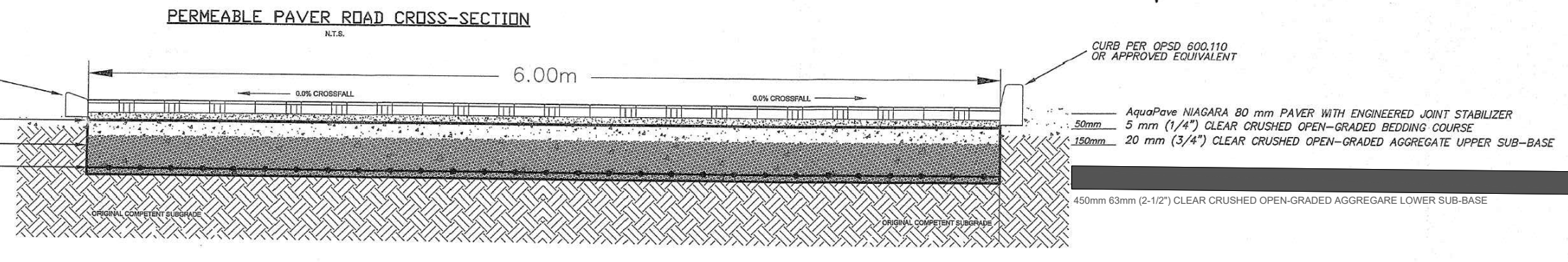
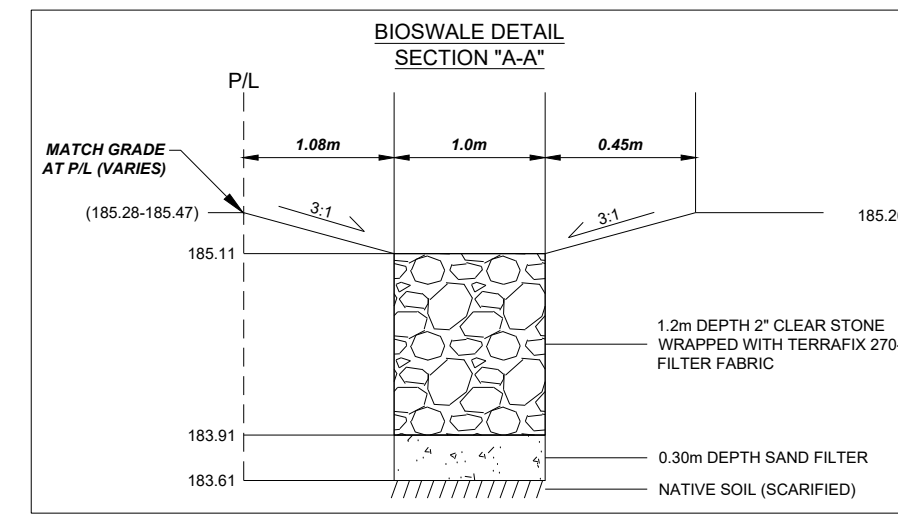
- GENERAL NOTES:**
- TENDERER SHALL SATISFY THEMSELVES AS TO THE NATURE OF THE GROUND AND BID ACCORDINGLY.
  - ALL ROCK LINE INDICATIONS SHOWN ON THE PLAN MUST BE VERIFIED BY THE CONTRACTOR.
  - CONTRACTOR SHALL VERIFY LOCATIONS AND INVERTS OF ALL EXISTING SANITARY AND STORM SEWERS AND WATERMANS, PRIVATE DRAINS AND WATER SERVICES, GAS MAINS, CABLE TV, HYDRO AND TELEPHONE DUCTS ETC AT START OF CONSTRUCTION.

NO.	DATE:	DESCRIPTION:
3	2023-09-20	ISSUED WITH FSR
2	2023-09-15	ISSUED WITH FSR
1	2023-09-05	ISSUED FOR CLIENT REVIEW
0	2023-03-15	ISSUED FOR FSR

REVISIONS

NO.	DATE:	DESCRIPTION:

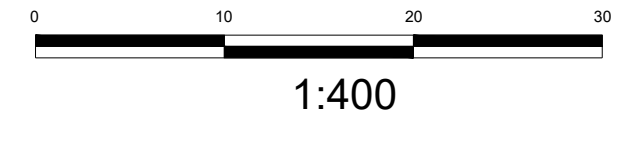
SEAL



APPROVAL OF THIS DRAWING IS FOR MATERIAL ACCEPTABILITY AND COMPLIANCE WITH MUNICIPAL AND PROVINCIAL SPECIFICATIONS AND STANDARDS ONLY. APPROVAL AND INSPECTION BY THE CITY OF THE WORKS DOES NOT CERTIFY THE LINE AND GRADE OF THE WORKS AND IT IS THE OWNER'S RESPONSIBILITY TO HAVE THEIR ENGINEER CERTIFY THIS ACCORDINGLY.

- NOTES re: SEPARATION DISTANCES:**
- MINIMUM HORIZONTAL SEPARATION BETWEEN WATER SERVICES / MAINS AND SEWER DRAINS AND MUNICIPAL SEWER MAINS SHALL BE 2.5M MEASURED FROM THE CLOSEST PIPE EDGE TO THE CLOSEST PIPE EDGE.
  - VERTICAL SEPARATION WHERE WATER SERVICE / MAIN PASSES OVER A SEWER DRAIN OR MUNICIPAL SEWER MAIN MUST BE A MINIMUM 0.20M UNLESS GREATER SEPARATION IS REQUIRED TO PROVIDE PROPER BEDDING AND STRUCTURAL SUPPORT. WATER SERVICES/MAINS PASSING UNDER SEWER DRAINS OR MUNICIPAL SEWER DRAINS MUST HAVE A SEPARATION OF 0.50M BETWEEN THE INVERT OF THE SEWER MAN/DRAIN AND THE CROWN OF THE WATER SERVICE/MAIN.

- LOCATIONS UNDERGROUND SERVICES ARE APPROXIMATE AND MUST BE FIELD VERIFIED PRIOR TO CONSTRUCTION.
- ANY DISCREPANCIES BETWEEN SERVICE LOCATIONS AND THESE ENGINEERING DRAWINGS MUST BE BROUGHT TO THE ATTENTION OF THE PROJECT ENGINEER.
- THIS PLAN SHALL BE INTERPRETED IN CONJUNCTION WITH THE SITE PLAN DRAWING PREPARED BY CUSIMANO ARCHITECT (LATEST VERSION). ANY DISCREPANCIES MUST BE BROUGHT TO THE ENGINEER'S ATTENTION IMMEDIATELY.



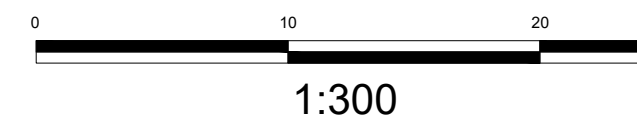
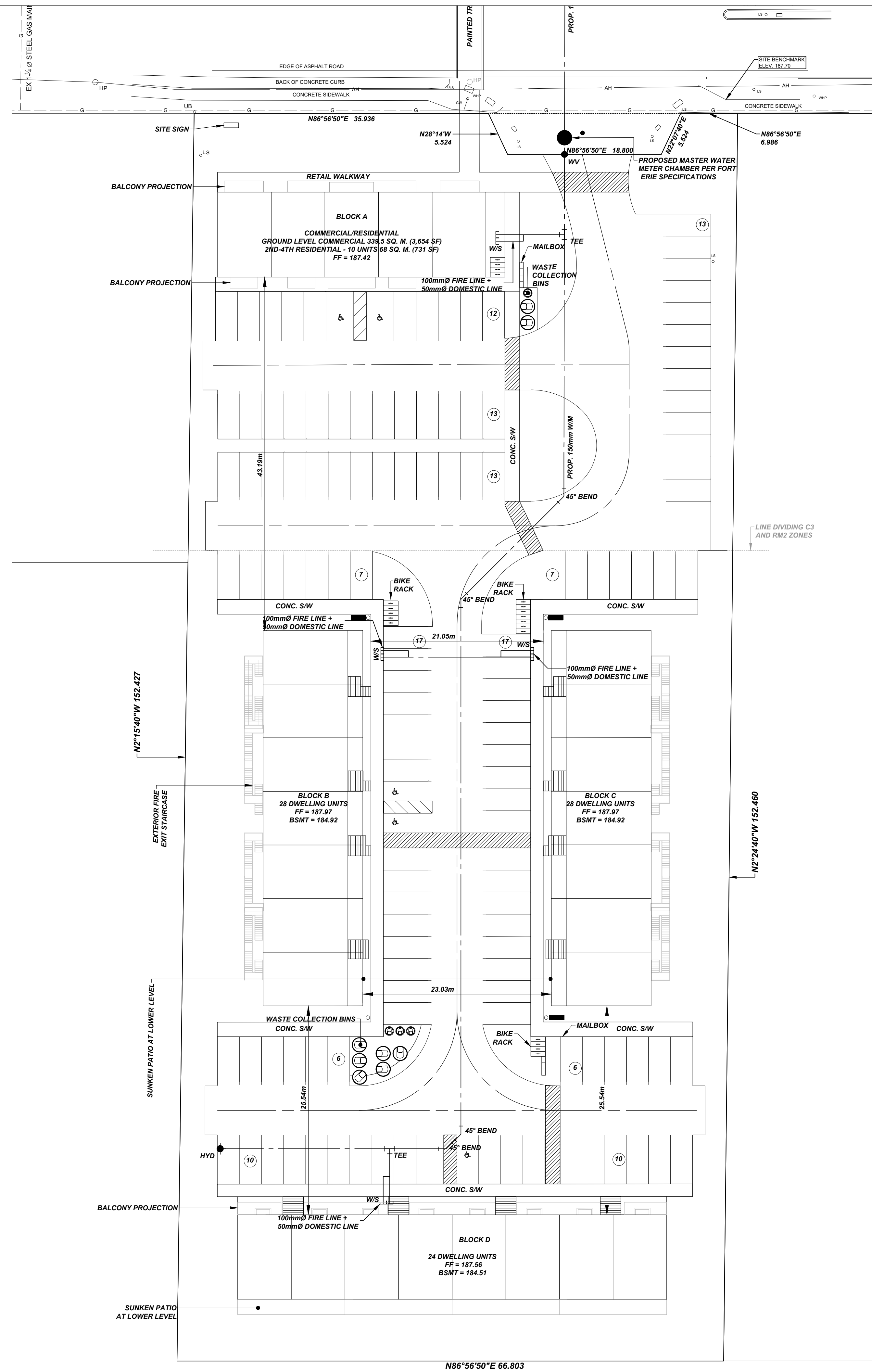
## Appendix 'B'

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Fire Protection Plan

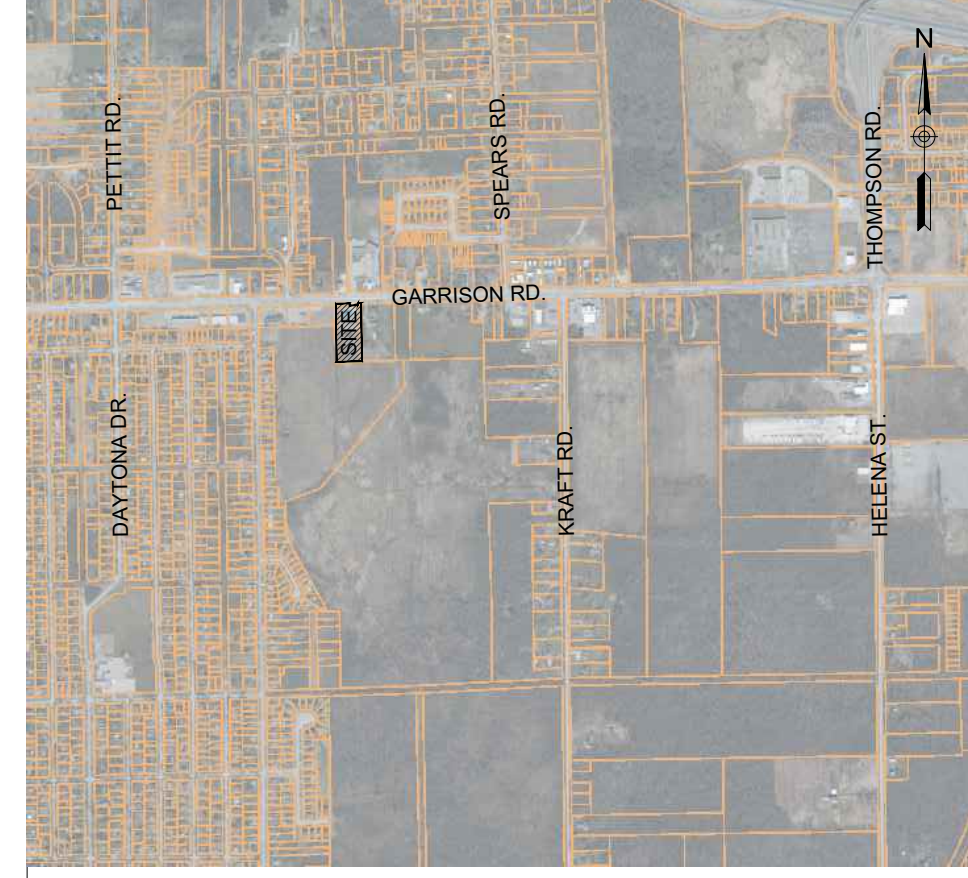
Fire Flow Requirement Calculations – Unit 1, 2, 3

Domestic Water Demand Calculations



**NOTES:**

1. LOCATIONS UNDERGROUND SERVICES ARE APPROXIMATE AND MUST BE FIELD VERIFIED PRIOR TO CONSTRUCTION.
2. ANY DISCREPANCIES BETWEEN SERVICE LOCATIONS AND THESE ENGINEERING DRAWINGS MUST BE BROUGHT TO THE ATTENTION OF THE PROJECT ENGINEER.
3. THIS PLAN SHALL BE INTERPRETED IN CONJUNCTION WITH THE SITE PLAN DRAWING PREPARED BY CUSIMANO ARCHITECT (LATEST VERSION). ANY DISCREPANCIES MUST BE BROUGHT TO THE ENGINEER'S ATTENTION IMMEDIATELY.



**KEY PLAN** N.T.S.

**BENCHMARK NOTE:**  
ELEVATIONS HEREON ARE ORTHOMETRIC AND ARE RELATED TO CGVD28, HT2, AS PREVIOUSLY ESTABLISHED BY THE LAROQUE GROUP.

**SITE BENCHMARK:**  
CONCRETE SIDEWALK CORNER, NORTH-EAST OF 1127 GARRISON ROAD.  
ELEVATION = 187.70m

- GENERAL NOTES:**
1. TENDERER SHALL SATISFY THEMSELVES AS TO THE NATURE OF THE GROUND AND BID ACCORDINGLY.
  2. ALL ROCK LINE INDICATIONS SHOWN ON THE PLAN MUST BE VERIFIED BY THE CONTRACTOR.
  3. CONTRACTOR SHALL VERIFY LOCATIONS AND INVERTS OF ALL EXISTING SANITARY AND STORM SEWERS AND WATERMANS, PRIVATE DRAINS AND WATER SERVICES, GAS MAINS, CABLE TV, HYDRO AND TELEPHONE DUCTS ETC AT START OF CONSTRUCTION.

NO.	DATE:	DESCRIPTION:
1	2023-09-20	ISSUED WITH FSR
0	2023-03-14	FIRST SUBMISSION

REVISIONS

SEAL

**LandSmith** ENGINEERING & CONSULTING LTD.  
1059 UPPER JAMES STREET, SUITE 207  
HAMILTON, ON L9C 3A6  
ANDREW@LANDSMITHEC.COM  
288-309-3632

CLIENT:  
**TRINITYSTAR AQUILA INC.**

MUNICIPALITY:  
**TOWN OF FORT ERIE**

PROJECT NAME:  
**1127 GARRISON RD.**

TITLE:  
**FIRE PROTECTION PLAN**

SCALE:	1:300	DATE:	2022-12-13
CHECKED BY:	AS	DESIGNED BY:	AS
DWG No:	220381SA	SHEET No:	5

**FIRE FLOW DEMAND REQUIREMENTS**

Project: 1127 Garrison Road, UNIT 1  
 Method: OFM-TG-03-1999  
 FIRE PROTECTION WATER SUPPLY GUIDELINE FOR PART 3 IN THE ONTARIO BUILDING CODE  
<http://www.mcscs.jus.gov.on.ca/english/FireMarshal/Legislation/TechnicalGuidelinesandReports/TG-1999-03.html>

Formula:

$$Q = K \times V \times S_{Tot}$$

Where: Q = minimum supply of water in litres  
 K = water supply coefficient (Table 1)  
 V = total building volume in cubic meters  
 S<sub>Tot</sub> = total of spacial coefficient tables

**Volume (V)**

**1st + 2nd + 3rd + 4th Floor**

Ground Floor Area: 543.33 (sq.m)  
 Height: 12 (m)  
 Volume 1 (Building): 6519.96 (cu.m)

**Total Volume (V) = 6520.0 (cu.m)**

**Water Supply Coefficient (K)**

K: 18

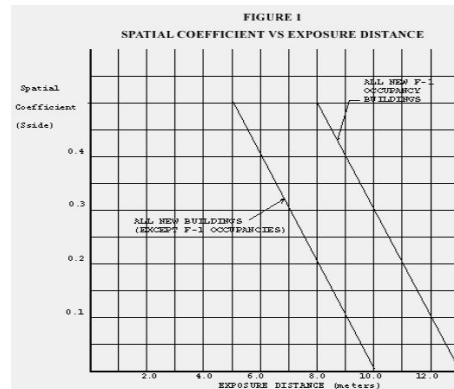
OBC Part: C (Residential)

Construction Type: *Building is of combustible construction with fire separations and fire-resistance ratings provided in accordance with Subsection 3.2.2. of the OBC, including loadbearing walls, columns and arches. Noncombustible construction may be used in lieu of fire-resistance rating where permitted in Subsection 3.2.2. of the OBC.*

**Spacial Coefficients (S)**

	Distance	
S <sub>1</sub>	0	25.4 (North)
S <sub>2</sub>	0	50 (East)
S <sub>3</sub>	0	50 (South)
S <sub>4</sub>	0	50 (West)

**S<sub>Tot</sub> = 1.0 + S<sub>1</sub> + S<sub>2</sub> + S<sub>3</sub> + S<sub>4</sub> = 1**



**Q = 117,360**

**Required Flow Rate (OBC) = 2,700 L / Min**  
 (See Table 2) = **45 L / Sec**

Building Code, Part 3 Buildings	Required Minimum Water Supply Flow Rate (L/min.)
One-storey building with building area not exceeding 600m <sup>2</sup> (excluding F-1 occupancies)	1800
All other buildings	2700 (If Q ≤ 108,000L) <sup>(1)</sup> 3600 (If Q > 108,000L and ≤ 135,000L) <sup>(1)</sup> 4500 (If Q > 135,000L and ≤ 162,000L) <sup>(1)</sup> 5400 (If Q > 162,000L and ≤ 190,000L) <sup>(1)</sup> 6300 (If Q > 190,000L and ≤ 270,000L) <sup>(1)</sup> 9000 (If Q > 270,000L) <sup>(1)</sup>

**FIRE FLOW DEMAND REQUIREMENTS**

Project: 1127 Garrison Road, UNIT 2  
 Method: OFM-TG-03-1999  
 FIRE PROTECTION WATER SUPPLY GUIDELINE FOR PART 3 IN THE ONTARIO BUILDING CODE  
<http://www.mcscs.jus.gov.on.ca/english/FireMarshal/Legislation/TechnicalGuidelinesandReports/TG-1999-03.html>

Formula:

$$Q = K \times V \times S_{Tot}$$

Where: Q = minimum supply of water in litres  
 K = water supply coefficient (Table 1)  
 V = total building volume in cubic meters  
 S<sub>Tot</sub> = total of spacial coefficient tables

**Volume (V)**

1st + 2nd + 3rd + 4th floor

Ground Floor Area: 475.4 (sq.m)  
 Height: 12 (m)  
 Volume 1 (Building): 5704.8 (cu.m)

**Total Volume (V) = 5704.8 (cu.m)**

**Water Supply Coefficient (K)**

K: 18

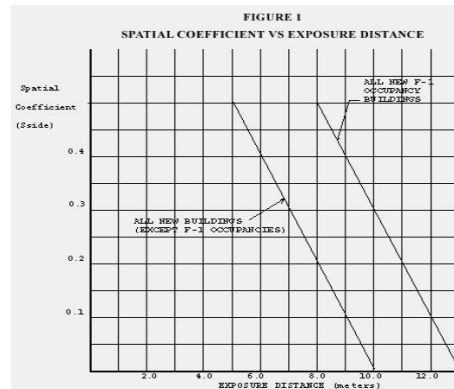
OBC Part: C (Residential)

Construction Type: *Building is of combustible construction with fire separations and fire-resistance ratings provided in accordance with Subsection 3.2.2. of the OBC, including loadbearing walls, columns and arches. Noncombustible construction may be used in lieu of fire-resistance rating where permitted in Subsection 3.2.2. of the OBC.*

**Spacial Coefficients (S)**

	Distance	
S <sub>1</sub>	0	45.2 (North)
S <sub>2</sub>	0	21.05 (East)
S <sub>3</sub>	0	25.4 (South)
S <sub>4</sub>	0	50 (West)

**S<sub>Tot</sub> = 1.0 + S<sub>1</sub> + S<sub>2</sub> + S<sub>3</sub> + S<sub>4</sub> = 1**



**Q = 102,686**

**Required Flow Rate (OBC) = 2,700 L / Min**  
 (See Table 2) = 45 L / Sec

Building Code, Part 3 Buildings	Required Minimum Water Supply Flow Rate (L/min.)
One-storey building with building area not exceeding 600m <sup>2</sup> (excluding F-1 occupancies)	1800
All other buildings	2700 (If Q ≤ 108,000L) <sup>(1)</sup> 3600 (If Q > 108,000L and ≤ 135,000L) <sup>(1)</sup> 4500 (If Q > 135,000L and ≤ 162,000L) <sup>(1)</sup> 5400 (If Q > 162,000L and ≤ 190,000L) <sup>(1)</sup> 6300 (If Q > 190,000L and ≤ 270,000L) <sup>(1)</sup> 9000 (If Q > 270,000L) <sup>(1)</sup>

**FIRE FLOW DEMAND REQUIREMENTS**

Project: 1127 Garrison Road, UNIT 2  
 Method: OFM-TG-03-1999  
 FIRE PROTECTION WATER SUPPLY GUIDELINE FOR PART 3 IN THE ONTARIO BUILDING CODE  
<http://www.mcscs.jus.gov.on.ca/english/FireMarshal/Legislation/TechnicalGuidelinesandReports/TG-1999-03.html>

Formula:

$$Q = K \times V \times S_{Tot}$$

Where: Q = minimum supply of water in litres  
 K = water supply coefficient (Table 1)  
 V = total building volume in cubic meters  
 S<sub>Tot</sub> = total of spacial coefficient tables

**Volume (V)**

1st + 2nd + 3rd + 4th floor

Ground Floor Area: 543.33 (sq.m)  
 Height: 12 (m)  
 Volume 1 (Building): 6519.96 (cu.m)

**Total Volume (V) = 6520.0 (cu.m)**

**Water Supply Coefficient (K)**

K: 18

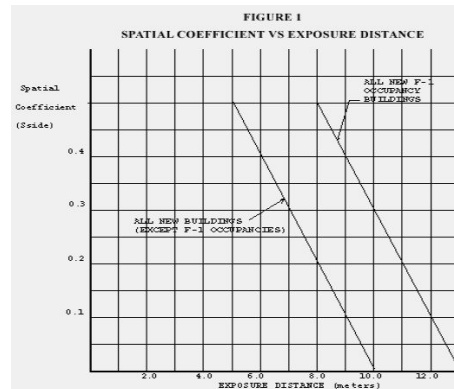
OBC Part: C (Residential)

Construction Type: *Building is of combustible construction with fire separations and fire-resistance ratings provided in accordance with Subsection 3.2.2. of the OBC, including loadbearing walls, columns and arches. Noncombustible construction may be used in lieu of fire-resistance rating where permitted in Subsection 3.2.2. of the OBC.*

**Spacial Coefficients (S)**

	Distance	
S <sub>1</sub>	0	45.2 (North)
S <sub>2</sub>	0	21.05 (East)
S <sub>3</sub>	0	25.4 (South)
S <sub>4</sub>	0	50 (West)

**S<sub>Tot</sub> = 1.0 + S<sub>1</sub> + S<sub>2</sub> + S<sub>3</sub> + S<sub>4</sub> = 1**



**Q = 117,360**

**Required Flow Rate (OBC) = 3,600 L / Min**  
 (See Table 2) = **60 L / Sec**

Building Code, Part 3 Buildings	Required Minimum Water Supply Flow Rate (L/min.)
One-storey building with building area not exceeding 600m <sup>2</sup> (excluding F-1 occupancies)	1800
All other buildings	2700 (If Q ≤ 108,000L) <sup>(1)</sup> 3600 (If Q > 108,000L and ≤ 135,000L) <sup>(1)</sup> 4500 (If Q > 135,000L and ≤ 162,000L) <sup>(1)</sup> 5400 (If Q > 162,000L and ≤ 190,000L) <sup>(1)</sup> 6300 (If Q > 190,000L and ≤ 270,000L) <sup>(1)</sup> 9000 (If Q > 270,000L) <sup>(1)</sup>



**DOMESTIC WATER USEAGE REQUIREMENTS**

Project: 1127 Garrison Road, Fort Erie  
 Method: Fixture Unit Method, Per OBC Table 7.6.3.2.A

**Fixtures:** The number of fixtures was calculated based on the Floor Plans by Organica Studio Inc. + dated Sept. 19, 2023

<u>Amount</u>	<u>Fixture Type</u>	<u>Fixture Units Per</u>	<u>Total</u>	
5	Public Bathroom Group	2.2	11	(Commercial Units)
33	Watercloset	2	66	
85	Private Bathroom Group	3.6	306	
29	Dishwasher	1.4	40.6	
60	Kitchen Sink	1.4	84	
60	Clothes Washer	1.4	84	
8	Hose Bib	2.5	20	
	Total:		<b>611.6</b>	<b>612</b>

1 - Reference Table 7.6.3.2.A, Ontario Building Code

**Hydraulic Load:** Fixture units are then transferred to Hydraulic Load based on Ontario Building Code Table 7.4.10.5.

Column 1	Column 2	Column 3	Column 4
<i>Fixture Units in service</i>	<i>Max Drainage Rate (Gal/m)</i>		
	Col. 1	Col. 1 × 10	Col. 1 × 100
100	53	174	900
90	51	164	835
80	49	153	750
70	47	140	680
60	44	128	600
50	41	115	520
40	38	102	435
30	33	88	350
20	27	72	262
10	21	53	174

Maximum hydraulic load is estimated to be 129 Imperial Gallons / Minute

612 Fixture Units = 9.77 L/s

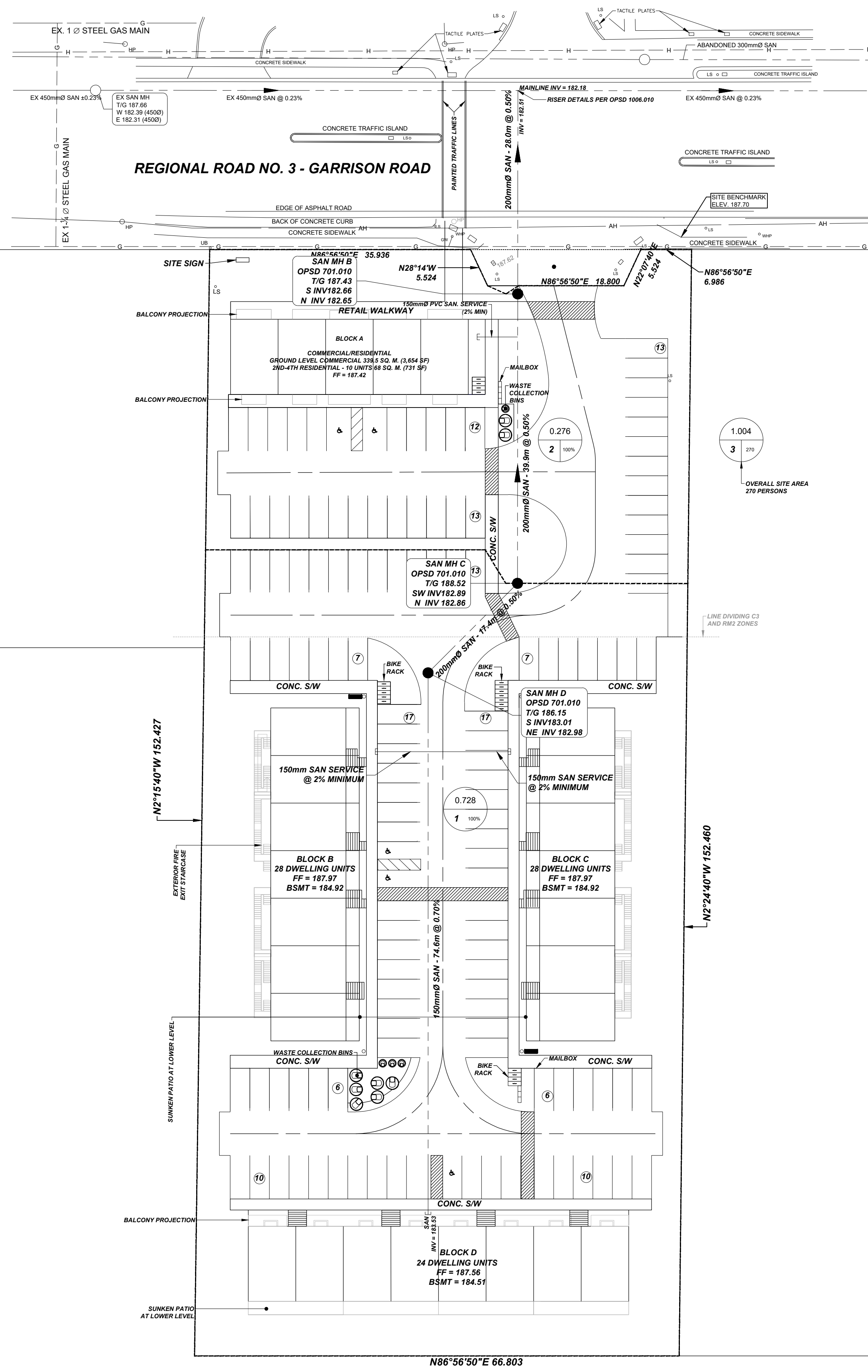
**The estimated maximum hydraulic load for the proposed development (90 Units) is 9.77 L/s**

## Appendix 'C'

---

Sanitary Drainage Area Plan

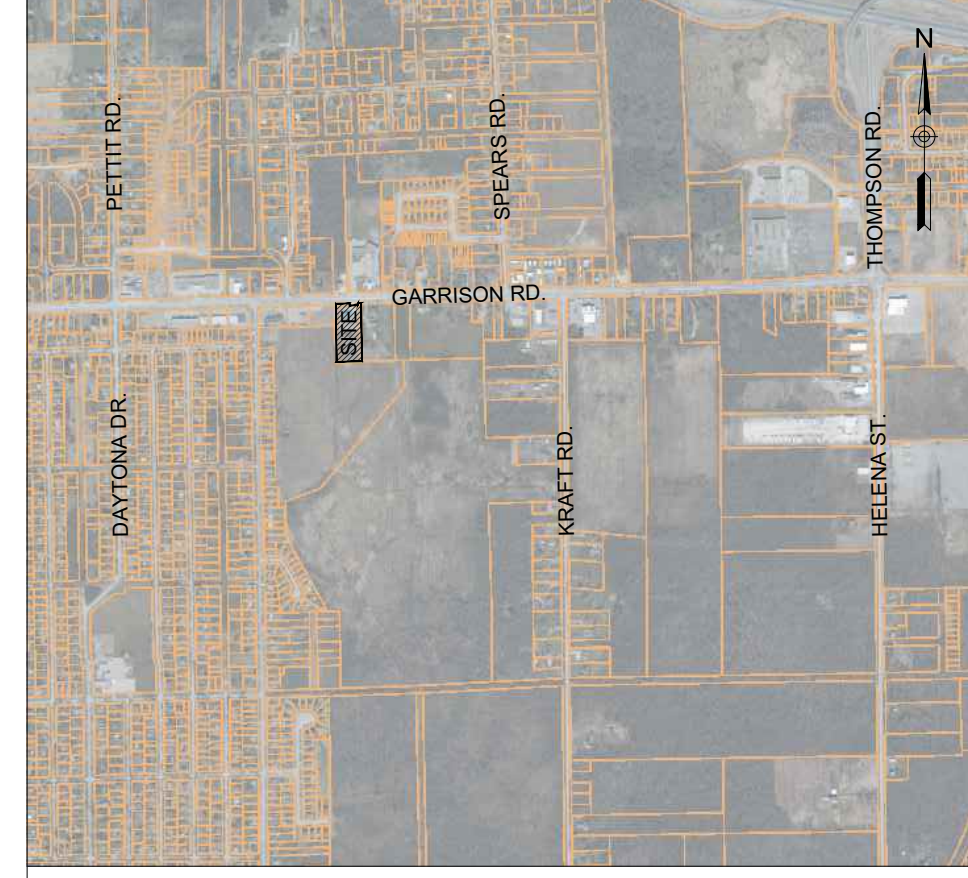
Pages from Niagara Region Water / Wastewater  
Master Servicing Plan (2016)



**LEGEND**

- EXISTING SANITARY
- PROPOSED SANITARY
- SAN
- SAN
- PLUG
- PLUG
- HYD
- FH

0.077 AREA (HECTARES)  
 1 141 POPULATION DENSITY  
 DRAINAGE AREA NO.



**KEY PLAN N.T.S.**

**BENCHMARK NOTE:**  
 ELEVATIONS HEREON ARE ORTHOMETRIC AND ARE RELATED TO CGVD28, HT2, AS PREVIOUSLY ESTABLISHED BY THE LAROQUE GROUP.

**SITE BENCHMARK:**  
 CONCRETE SIDEWALK CORNER, NORTH-EAST OF 1127 GARRISON ROAD.  
 ELEVATION = 187.70

- GENERAL NOTES:**
- TENDERER SHALL SATISFY THEMSELVES AS TO THE NATURE OF THE GROUND AND BID ACCORDINGLY.
  - ALL ROCK LINE INDICATIONS SHOWN ON THE PLAN MUST BE VERIFIED BY THE CONTRACTOR.
  - CONTRACTOR SHALL VERIFY LOCATIONS AND INVERTS OF ALL EXISTING SANITARY AND STORM SEWERS AND WATERMANS, PRIVATE DRAINS AND WATER SERVICES, GAS MAINS, CABLE TV, HYDRO AND TELEPHONE DUCTS ETC AT START OF CONSTRUCTION.

NO.	DATE:	DESCRIPTION:
1	2023-09-21	ISSUED WITH FSR
0	2023-03-14	FIRST SUBMISSION

REVISIONS

SEAL

**LandSmith** ENGINEERING & CONSULTING LTD.  
 1059 UPPER JAMES STREET, SUITE 207  
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 ANDREW@LANDSMITHEC.COM  
 288-309-3632

CLIENT:  
**TRINITYSTAR AQUILA INC.**

MUNICIPALITY:  
**TOWN OF FORT ERIE**

PROJECT NAME:  
**1127 GARRISON RD.**

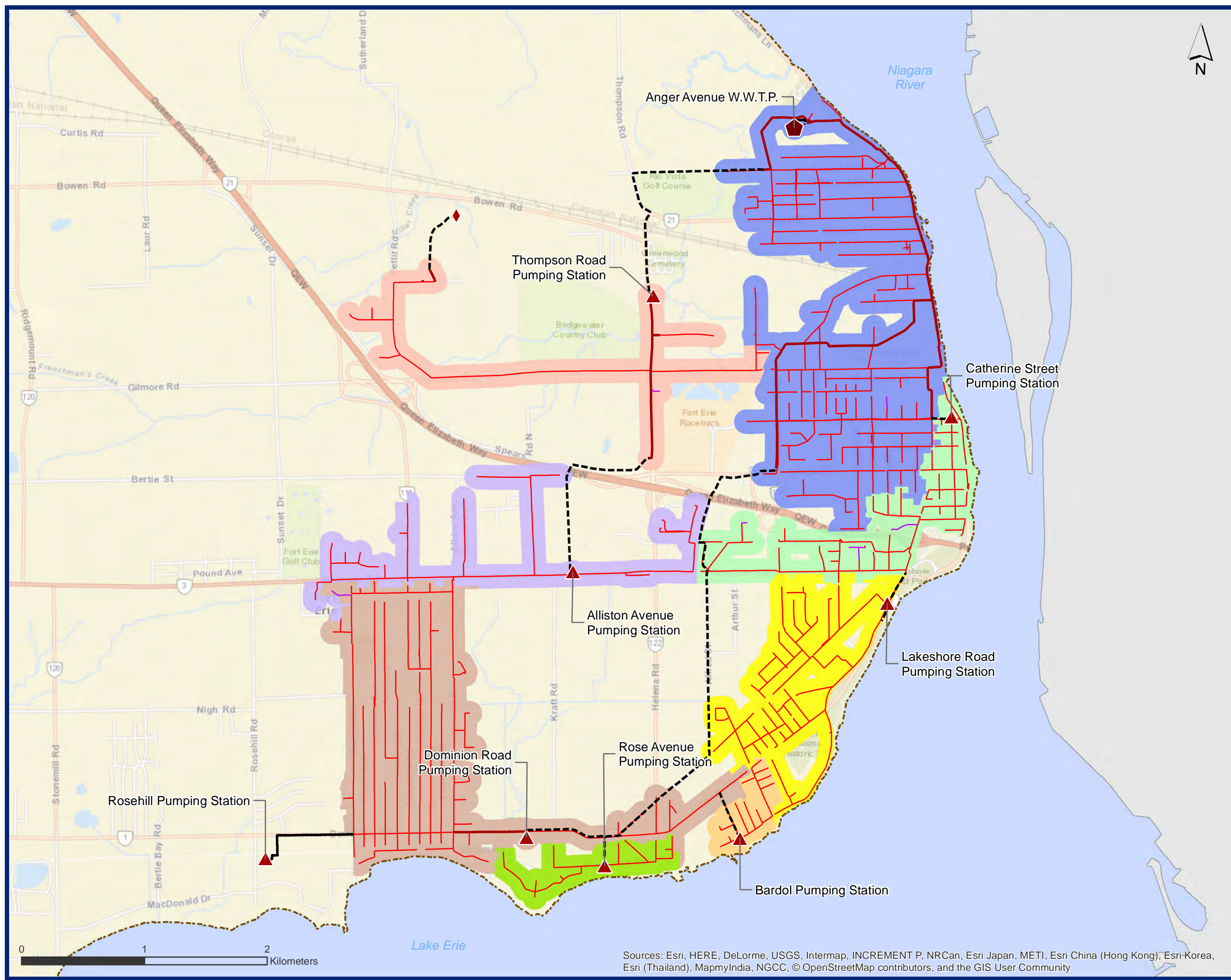
TITLE:  
**SANITARY DRAINAGE AREA PLAN**

SCALE:	1:400	DATE:	2022-09-29
CHECKED BY:	AS	DESIGNED BY:	BC
DWG No:	220381SA	SHEET No:	6

APPROVAL OF THIS DRAWING IS FOR MATERIAL ACCEPTABILITY AND COMPLIANCE WITH MUNICIPAL AND PROVINCIAL SPECIFICATIONS AND STANDARDS ONLY. APPROVAL AND INSPECTION BY THE CITY OF THE WORKS DOES NOT CERTIFY THE LINE AND GRADE OF THE WORKS AND IT IS THE OWNER'S RESPONSIBILITY TO HAVE THEIR ENGINEER CERTIFY THIS ACCORDINGLY.

- NOTES re: SEPARATION DISTANCES:**
- MINIMUM HORIZONTAL SEPARATION BETWEEN WATER SERVICES / MANS AND SEWER DRAINS AND MUNICIPAL SEWER MAINS SHALL BE 2.5M MEASURED FROM THE CLOSEST PIPE EDGE TO THE CLOSEST PIPE EDGE.
  - VERTICAL SEPARATION WHERE WATER SERVICE / MAIN PASSES OVER A SEWER DRAIN OR MUNICIPAL SEWER MAIN MUST BE A MINIMUM 0.20M UNLESS GREATER SEPARATION IS REQUIRED TO PROVIDE PROPER BEDDING AND STRUCTURAL SUPPORT. WATER SERVICES/MANS PASSING UNDER SEWER DRAINS OR MUNICIPAL SEWER DRAINS MUST HAVE A SEPARATION OF 0.50M BETWEEN THE INVERT OF THE SEWER MAIN/DRAIN AND THE CROWN OF THE WATER SERVICE/MAN.

- NOTES:**
- LOCATIONS UNDERGROUND SERVICES ARE APPROXIMATE AND MUST BE FIELD VERIFIED PRIOR TO CONSTRUCTION.
  - ANY DISCREPANCIES BETWEEN SERVICE LOCATIONS AND THESE ENGINEERING DRAWINGS MUST BE BROUGHT TO THE ATTENTION OF THE PROJECT ENGINEER.
  - THIS PLAN SHALL BE INTERPRETED IN CONJUNCTION WITH THE SITE PLAN DRAWING PREPARED BY CUSIMANO ARCHITECT (LATEST VERSION). ANY DISCREPANCIES MUST BE BROUGHT TO THE ENGINEER'S ATTENTION IMMEDIATELY.



Wastewater Facilities

- |                                    |                             |
|------------------------------------|-----------------------------|
| Wastewater Treatment Plant         | Regional Pumping Station    |
| Combined Sewage Detention Facility | Municipal Pumping Station   |
| Lagoon                             | Private Pumping Station     |
| Odour Control Facility             | Regional Wastewater Network |
| Leachate Pumping Station           | Local Wastewater Network    |
|                                    | Private Wastewater Network  |
|                                    | Forcemain                   |

Wastewater Catchments\*

\*Catchment limits are shown based on property boundaries and are within 100 m of sewers.

- |                       |                |
|-----------------------|----------------|
| Anger Avenue W.W.T.P. | Dominion Road  |
| Alliston Avenue       | Lakeshore Road |
| Bardol                | Rose Avenue    |
| Catherine Street      | Thompson Road  |

Figure 4.H.1  
Existing Wastewater System  
Anger Avenue WWTP



Sources: Esri, HERE, DeLorme, USGS, Intermap, INCREMENT P, NRCan, Esri Japan, METI, Esri China (Hong Kong), Esri-Korea, Esri (Thailand), MapmyIndia, NGCC, © OpenStreetMap contributors, and the GIS User Community

**Table 4.H.7 Existing Wastewater System Flows by Catchment**

Catchment	Total Service Equivalent Population	Existing Average Dry Weather Flow (L/s)	Existing Design Peak Wet Weather Flow (L/s)	Existing 2-Year Flow (L/s)	Existing 5-Year Flow (L/s)
<b>Anger Avenue Wastewater Treatment Plant (WWTP)</b>	25,431	136.7	657.5	784.6	841.6
<b>Anger Avenue WWTP</b>	10,702	75.9	272.2	340.0	420.0
<b>Thompson Road Sewage Pumping Station (SPS)</b>	6,579	19.0	116.5	169.0	226.0
Thompson Road SPS	2,104	13.2	64.0	122.0	164.0
Alliston Avenue SPS	4,475	5.8	52.5	47.0	62.0
<b>Catherine Street SPS</b>	2,783	24.4	125.8	180.0	270.0
Catherine Street SPS	1,324	17.0	69.1	77.0	126.0
Lakeshore SPS	1,459	7.4	56.7	103.0	144.0
<b>Dominion Road SPS</b>	5,366	17.4	143.0	1107.0	1540.0
Dominion Road SPS	4,686	13.4	114.2	897.5	1248.5
Rose Avenue SPS	363	1.6	16.1	129.0	179.5
Bardol SPS	317	2.4	12.7	80.5	112.0

Note: Flow numbers may not sum due to rounding.

**Table 4.H.10 Projected Peak Dry Weather Flow by Catchment**

Catchment	2021 Design Peak Dry Weather Flow (L/s)	2026 Design Peak Dry Weather Flow (L/s)	2031 Design Peak Dry Weather Flow (L/s)	2036 Design Peak Dry Weather Flow (L/s)	2041 Design Peak Dry Weather Flow (L/s)
Anger Avenue Wastewater Treatment Plant	153.5	160.4	168.8	189.5	200.0
Alliston Avenue Sewage Pumping Station (SPS)	14.2	18.3	19.8	21.3	23.4
Bardol SPS	5.3	6.6	7.7	8.7	9.1
Catherine Street SPS	34.5	35.2	35.8	35.9	36.2
Dominion Road SPS	29.0	34.5	38.1	40.3	41.5
Lakeshore Road SPS	15.6	18.3	20.2	21.9	22.7
Rose Avenue SPS	3.4	4.3	5.1	5.6	5.8
Thompson Road SPS	35.3	40.4	46.8	53.8	60.9
<b>Total</b>	<b>290.9</b>	<b>318.1</b>	<b>342.3</b>	<b>377.1</b>	<b>399.5</b>

The following presents an example calculation of projected peak dry weather flow.

2041 Peak Dry Weather Flow for Lakeshore Road Sewage Pumping Station:  
 = (2014 Average Dry Weather Flow × Peaking Factor) +  
 (2041 Equivalent Population – 2014 Equivalent Population) × 275 L/cap/day ×  
 1 day/86400 s × Harmon Peaking Factor for Growth Population  
 = (7.41 L/s × 2.0) + (2,155 – 1,459 people) × 275 L/cap/day × 1 day/86400 s × 3.56  
 = 22.7 L/s

**Table 4.H.11 Projected Peak Wet Weather Flow by Catchment**

Catchment	2021 Design Peak Wet Weather Flow (L/s)	2026 Design Peak Wet Weather Flow (L/s)	2031 Design Peak Wet Weather Flow (L/s)	2036 Design Peak Wet Weather Flow (L/s)	2041 Design Peak Wet Weather Flow (L/s)
Anger Avenue Wastewater Treatment Plant	273.9	280.7	289.1	309.9	320.3
Alliston Avenue Sewage Pumping Station (SPS)	55.1	59.2	60.7	62.3	64.3
Bardol SPS	13.1	14.4	15.6	16.5	16.9
Catherine Street SPS	69.7	70.4	70.9	71.1	71.4
Dominion Road SPS	116.5	121.9	125.5	127.7	128.9
Lakeshore Road SPS (Fort Erie)	57.5	60.2	62.1	63.8	64.6
Rose Avenue SPS	16.2	17.2	18.0	18.5	18.7
Thompson Road SPS	72.9	78.1	84.4	91.4	98.5
<b>Total</b>	<b>675.0</b>	<b>702.1</b>	<b>726.4</b>	<b>761.2</b>	<b>783.6</b>

The following presents an example calculation of projected peak wet weather flow.

2041 Peak Wet Weather Flow for Lakeshore Road Sewage Pumping Station:  
 = 2041 Peak Dry Weather Flow + 2041 Design RDII  
 = 2041 Peak Dry Weather Flow + (2041 Catchment Area × 0.286 L/s/ha)  
 = 22.7 L/s + (146.4 ha × 0.286 L/s/ha)  
 = 64.6 L/s

**Table 4.H.12 System Sewage Pumping Station Performance**

Sewage Pumping Station	Contributing Catchments	Facility Operational Capacity (L/s)	Existing Design Peak Wet Weather Flow (L/s)	2041 Design Peak Wet Weather Flow (L/s)	2041 Surplus/Deficit (L/s)
Thompson Road Sewage Pumping Station (SPS)	Thompson Road SPS (Including Sub Catchments) Alliston Avenue SPS	298.0	116.5	158.6	139.4
Alliston Avenue SPS	Alliston Avenue SPS	43.0	52.5	64.3	-21.3
Catherine Street SPS	Catherine Street SPS (Including Sub Catchments) Lakeshore Road SPS	117.0	125.8	135.3	-18.3
Lakeshore Road SPS	Lakeshore Road SPS	63.0	56.7	64.6	-1.6
Dominion Road SPS	Dominion Road SPS (Including Sub Catchments) Rose Avenue SPS Bardol SPS	215.0	143.0	162.7	52.3
Rose Avenue SPS	Rose Avenue SPS	48.0	16.1	18.7	29.3
Bardol SPS	Bardol SPS	45.0	12.7	16.9	28.1

The following sewage pumping stations have projected pumping deficits:

- Alliston Avenue Sewage Pumping Station
- Catherine Street Sewage Pumping Station
- Lakeshore Road Sewage Pumping Station



**Table 4.H.14 Summary of Anger Avenue Wastewater Treatment Plant Capital Program**

Master Plan ID	Name	Description	Size / Capacity	Year in Service	Municipality	Class EA Schedule	Class EA Status	Project Type	Total Component Estimated Cost
WW-FM-001	Upgrade Catherine Street Sewage Pumping Station (SPS) Forcemain	Upgrade Catherine Street SPS Forcemain in Fort Erie	300 mm	2032-2041	Fort Erie	A+	Satisfied	Forcemain	\$467,000
WW-II-001	Wet weather reduction in East Fort Erie	Wet weather reduction in East Fort Erie	30 L/s reduction	2022-2031	Fort Erie	N/A	Dependent on outcome of wet weather flow study	Wet Weather Reduction	\$4,500,000
WW-SPS-001	Alliston Avenue SPS Pump Replacement - Anger Avenue	Increase station capacity from 43 L/s to 129 L/s.	129 L/s	2022-2031	Fort Erie	A+	Satisfied	Pumping	\$989,000
WW-SPS-002	Catherine Street SPS Expansion - Anger Avenue	Increase station capacity from 117 L/s to 140 L/s	140 L/s	2032-2041	Fort Erie	A+	Satisfied	Pumping	\$2,945,000
WW-SPS-003	Lakeshore Road SPS Upgrade - Anger Avenue	Increase station capacity from 63 L/s to 70 L/s	70 L/s	2022-2031	Fort Erie	A+	Satisfied	Pumping	\$2,618,000
<b>Total</b>									<b>\$11,519,000</b>

## Appendix 'D'

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Pre-Development Drainage Area Plan

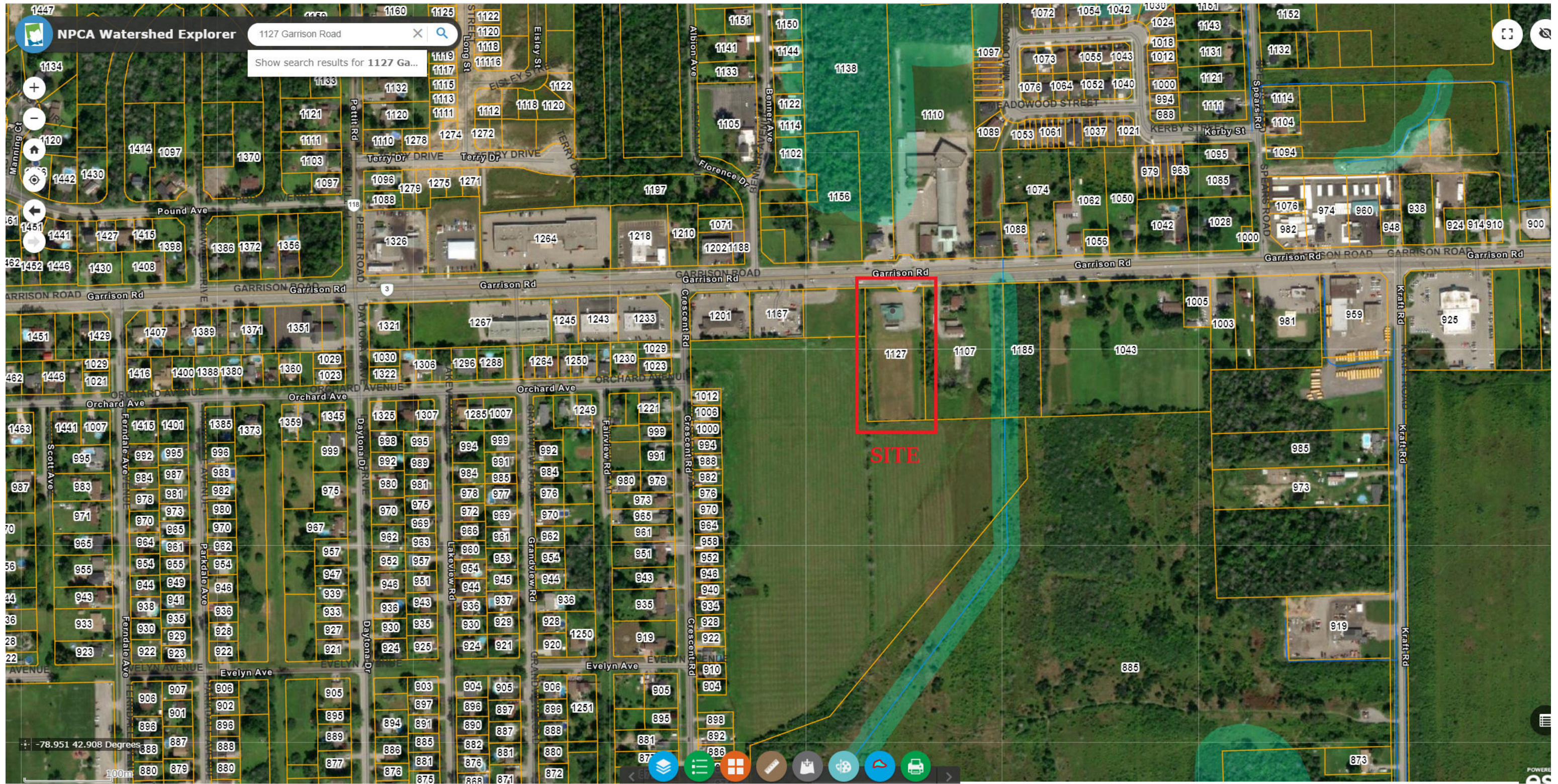
NPCA Figure re: Drainage Context

Post-Development Drainage Area Plan

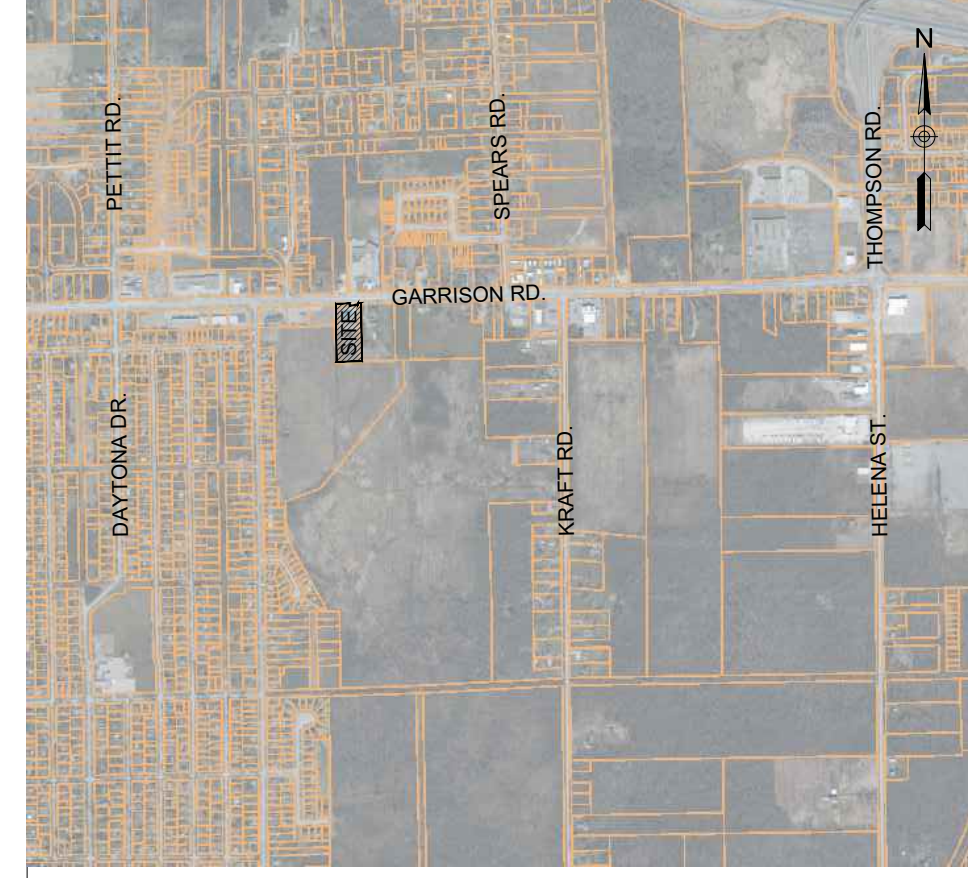
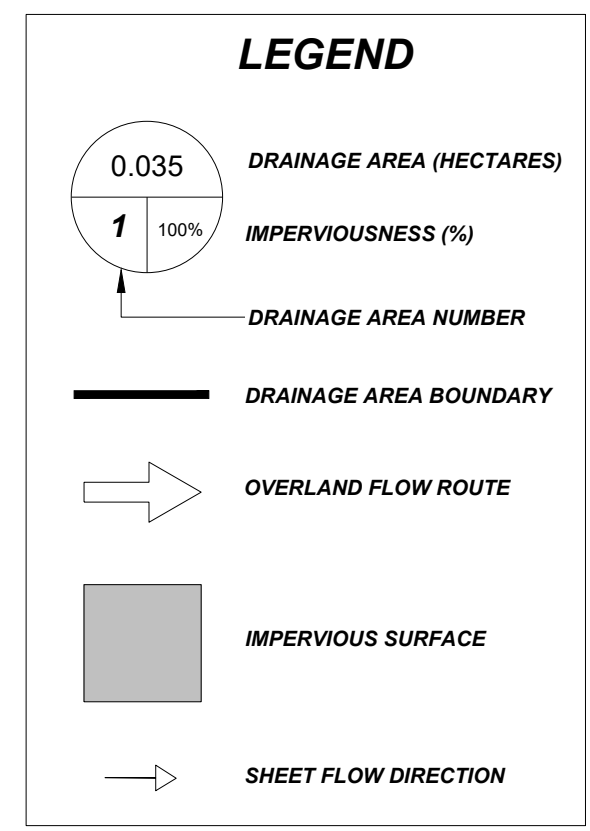
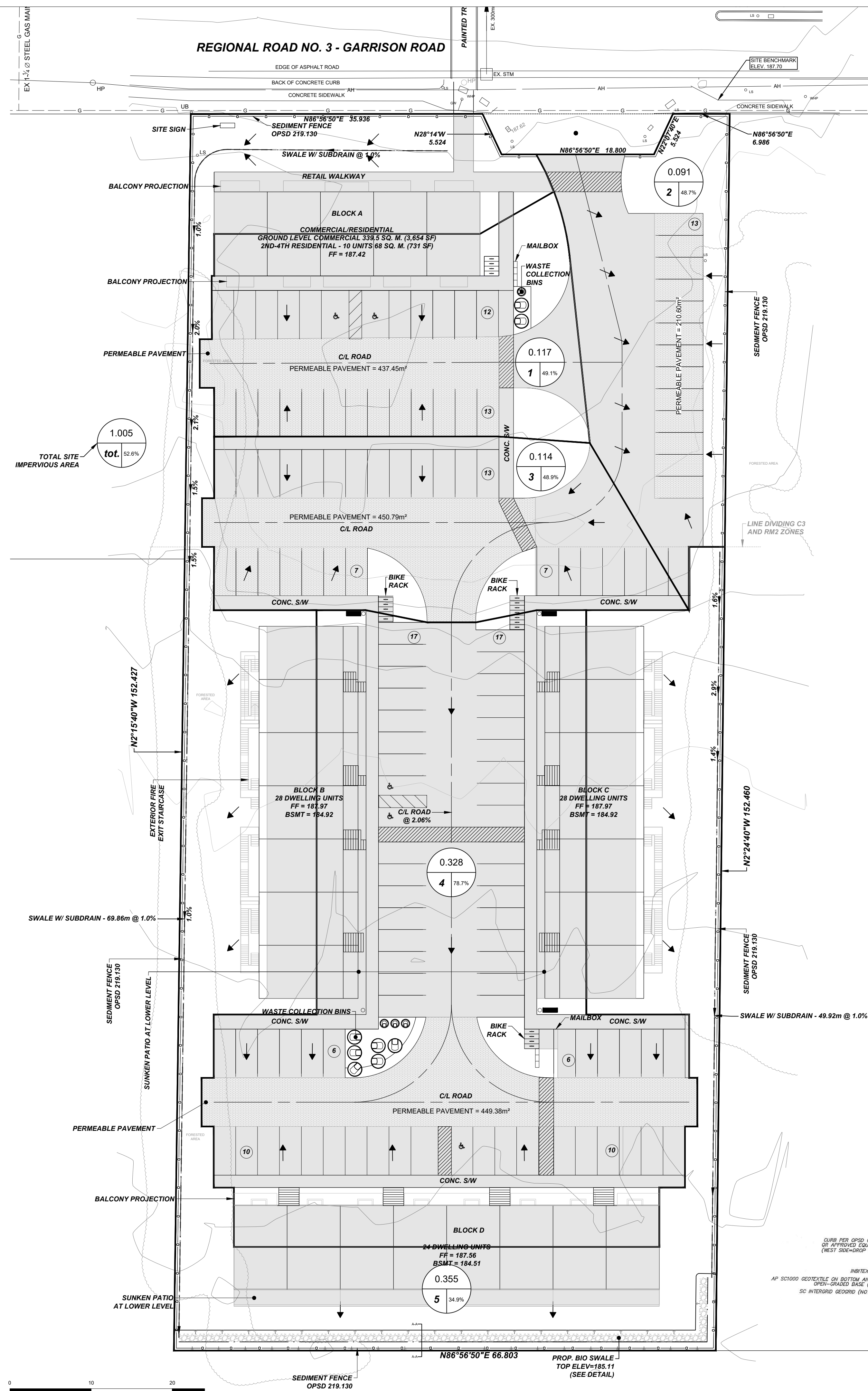
Permeable Paver Fact Sheet

Bio-Swale Fact Sheet





1127 Garrison Road, NPCA Watershed Explorer, Storm Drainage Context



**KEY PLAN** N.T.S.

BENCHMARK NOTE:  
ELEVATIONS HEREON ARE ORTHOMETRIC AND ARE RELATED TO CGVD28, HT2, AS PREVIOUSLY ESTABLISHED BY THE LAROQUE GROUP.

SITE BENCHMARK:  
CONCRETE SIDEWALK CORNER, NORTH-EAST OF 1127 GARRISON ROAD.  
ELEVATION = 187.70m

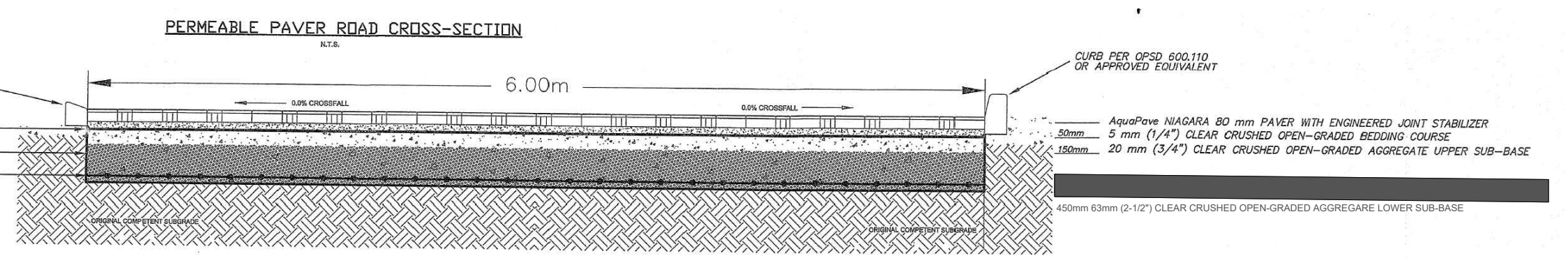
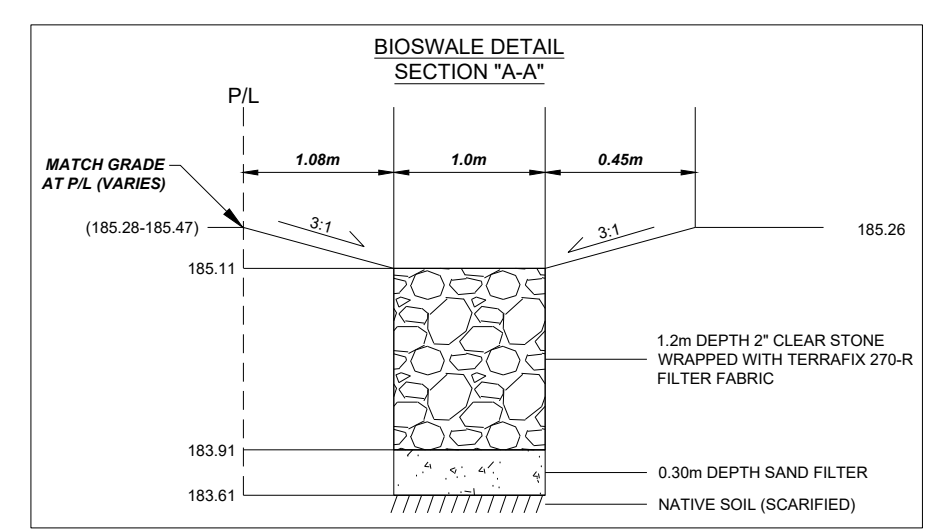
- GENERAL NOTES:
- TENDERER SHALL SATISFY THEMSELVES AS TO THE NATURE OF THE GROUND AND BID ACCORDINGLY.
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  - CONTRACTOR SHALL VERIFY LOCATIONS AND INVERTS OF ALL EXISTING SANITARY AND STORM SEWERS AND WATERMANS, PRIVATE DRAINS AND WATER SERVICES, GAS MAINS, CABLE TV, HYDRO AND TELEPHONE DUCTS ETC AT START OF CONSTRUCTION.

NO:	DATE:	DESCRIPTION:
1	2023-09-21	ISSUED WITH FSR
0	2023-03-14	FIRST SUBMISSION

REVISIONS	

**LandSmith** ENGINEERING & CONSULTING LTD.  
 LANDSMITH ENGINEERING & CONSULTING LTD.  
 1059 UPPER JAMES STREET, SUITE 207  
 HAMILTON, ON L9C 3A6  
 ANDREW@LANDSMITHEC.COM  
 288-309-3632

CLIENT:	TRINITYSTAR AQUILA INC.
MUNICIPALITY:	TOWN OF FORT ERIE
PROJECT NAME:	1127 GARRISON RD.
TITLE:	POST-DEVELOPMENT DRAINAGE AREA PLAN
SCALE:	1:300
DATE:	2022-12-13
CHECKED BY:	AS
DESIGNED BY:	AS
DWG No:	220381SA
SHEET No:	4



- NOTES:
- LOCATIONS UNDERGROUND SERVICES ARE APPROXIMATE AND MUST BE FIELD VERIFIED PRIOR TO CONSTRUCTION.
  - ANY DISCREPANCIES BETWEEN SERVICE LOCATIONS AND THESE ENGINEERING DRAWINGS MUST BE BROUGHT TO THE ATTENTION OF THE PROJECT ENGINEER.
  - THIS PLAN SHALL BE INTERPRETED IN CONJUNCTION WITH THE SITE PLAN DRAWING PREPARED BY CUSIMANO ARCHITECT (LATEST VERSION). ANY DISCREPANCIES MUST BE BROUGHT TO THE ENGINEER'S ATTENTION IMMEDIATELY.

TOTAL P.P. AREA = 1,558.59m<sup>2</sup>  
 P.P. VOLUME = 285m<sup>3</sup>  
 BIO-SWALE VOLUME = 35m<sup>3</sup>

1:300

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"          Job folder:                   Z:\Project Files\PROJECTS\Fort Erie\
"          1127 Garrison Road, Fort Erie\SWM Calculations"
"          Output filename:              Pre-100year.out"
"          Licensee name:                Andrew Smith"
"          Company                       LandSmith Engineering & Consulting Ltd."
"          Date & Time last used:        2023-03-14 at 2:12:57 PM"
" 31          TIME PARAMETERS"
"          5.000  Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32          STORM Chicago storm"
"          1  Chicago storm"
"          1083.550 Coefficient A"
"          6.618  Constant B"
"          0.735  Exponent C"
"          0.500  Fraction R"
"          180.000 Duration"
"          1.000  Time step multiplier"
"          Maximum intensity              137.317  mm/hr"
"          Total depth                    69.634  mm"
"          6  100hyd Hydrograph extension used in this file"
" 33          CATCHMENT 101"
"          1  Triangular SCS"
"          1  Equal length"
"          1  SCS method"
"          101 No description"
"          15.000 % Impervious"
"          1.005  Total Area"
"          80.000 Flow length"
"          2.000  Overland Slope"
"          0.854  Pervious Area"
"          80.000 Pervious length"
"          2.000  Pervious slope"
"          0.151  Impervious Area"
"          80.000 Impervious length"
"          2.000  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000 Pervious SCS Curve No."
"          0.368  Pervious Runoff coefficient"
"          0.100  Pervious Ia/S coefficient"
"          8.467  Pervious Initial abstraction"
"          0.015  Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.900  Impervious Runoff coefficient"
"          0.100  Impervious Ia/S coefficient"
"          0.518  Impervious Initial abstraction"
"          0.078  0.000  0.000  0.000 c.m/sec"
"          Catchment 101  Pervious  Impervious  Total Area  "
"          Surface Area      0.854  0.151  1.005  hectare"
"          Time of concentration  25.692  3.539  19.011  minutes"
"          Time to Centroid      142.989  101.881  130.592  minutes"
"          Rainfall depth      69.634  69.634  69.634  mm"
"          Rainfall volume      594.85  104.97  699.82  c.m"
"          Rainfall losses      44.016  6.953  38.457  mm"
"          Runoff depth         25.618  62.681  31.177  mm"
"          Runoff volume        218.84  94.49  313.33  c.m"
"          Runoff coefficient    0.368  0.900  0.448  "
"          Maximum flow         0.064  0.057  0.078  c.m/sec"
" 40          HYDROGRAPH Add Runoff "
"          4  Add Runoff "
"          0.078  0.078  0.000  0.000"

```



```

"          MIDUSS Output ----->"
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"          MIDUSS created                 February 7, 2010"
"          10 Units used:                 ie METRIC"
"          Job folder:                   Z:\Project Files\PROJECTS\Fort Erie\
"                                     1127 Garrison Road, Fort Erie\SWM Calculations"
"          Output filename:              Post_2year_fixed.out"
"          Licensee name:                Andrew Smith"
"          Company                       LandSmith Engineering & Consulting Ltd."
"          Date & Time last used:        2023-03-14 at 2:54:54 PM"
" 31          TIME PARAMETERS"
"          5.000 Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32          STORM Chicago storm"
"          1 Chicago storm"
"          628.050 Coefficient A"
"          6.652 Constant B"
"          0.796 Exponent C"
"          0.500 Fraction R"
"          180.000 Duration"
"          1.000 Time step multiplier"
"          Maximum intensity              66.943 mm/hr"
"          Total depth                    29.334 mm"
"          6 002hyd Hydrograph extension used in this file"
" 33          CATCHMENT 101"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          101 No description"
"          70.000 % Impervious"
"          1.005 Total Area"
"          80.000 Flow length"
"          1.000 Overland Slope"
"          0.302 Pervious Area"
"          80.000 Pervious length"
"          1.000 Pervious slope"
"          0.703 Impervious Area"
"          80.000 Impervious length"
"          1.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          75.000 Pervious SCS Curve No."
"          0.141 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          8.467 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.828 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.112 0.000 0.000 0.000 c.m/sec"
"          Catchment 101 Pervious Impervious Total Area "
"          Surface Area 0.302 0.703 1.005 hectare"
"          Time of concentration 61.758 5.910 9.701 minutes"
"          Time to Centroid 192.168 107.539 113.283 minutes"
"          Rainfall depth 29.334 29.334 29.334 mm"
"          Rainfall volume 88.44 206.37 294.81 c.m"
"          Rainfall losses 25.208 5.049 11.097 mm"
"          Runoff depth 4.126 24.285 18.237 mm"
"          Runoff volume 12.44 170.84 183.28 c.m"
"          Runoff coefficient 0.141 0.828 0.622 "
"          Maximum flow 0.002 0.112 0.112 c.m/sec"
" 40          HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.112 0.112 0.000 0.000"
" 54          POND DESIGN"
"          0.112 Current peak flow c.m/sec"
"          0.078 Target outflow c.m/sec"
"          183.3 Hydrograph volume c.m"
"          11. Number of stages"

```

```

"      0.000  Minimum water level  metre"
"      1.500  Maximum water level  metre"
"      0.000  Starting water level  metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge  Volume"
"          0.000  0.000  0.000"
"          0.1500 1.00E-07 33.000"
"          0.3000 1.00E-07 66.000"
"          0.4500 1.00E-07 99.000"
"          0.6000 0.01027 132.000"
"          0.7500 0.03866 165.000"
"          0.9000 0.05381 198.000"
"          1.050  0.06555 231.000"
"          1.200  0.07549 264.000"
"          1.350  0.08426 297.000"
"          1.500  0.09220 330.000"
(NOTE RATING CURVE DOES NOT REFLECT SITE DESIGN, ADDED FOR VOLUME ESTIMATES ONLY)
"      1.  ORIFICES"
"          Orifice Orifice Orifice Number of"
"          invert coefficie diameter orifices"
"          0.450  0.630  0.2100  1.000"
"          Peak outflow 0.011 c.m/sec"
"          Maximum level 0.604 metre"
"          Maximum storage 132.983 c.m"
"          Centroidal lag 3.201 hours"
"          0.112  0.112  0.011  0.000 c.m/sec"

```

```

"          MIDUSS Output ----->"
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"          MIDUSS created                      February 7, 2010"
"          10  Units used:                      ie METRIC"
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"          1127 Garrison Road, Fort Erie\SWM Calculations"
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"          Licensee name:                      Andrew Smith"
"          Company                            LandSmith Engineering & Consulting Ltd."
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" 31      TIME PARAMETERS"
"          5.000  Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"          1  Chicago storm"
"          747.930 Coefficient A"
"          6.800  Constant B"
"          0.768  Exponent C"
"          0.500  Fraction R"
"          180.000 Duration"
"          1.000  Time step multiplier"
"          Maximum intensity          85.669  mm/hr"
"          Total depth                40.417  mm"
"          6  005hyd Hydrograph extension used in this file"
" 33      CATCHMENT 101"
"          1  Triangular SCS"
"          1  Equal length"
"          1  SCS method"
"          101  No description"
"          70.000 % Impervious"
"          1.005 Total Area"
"          80.000 Flow length"
"          1.000 Overland Slope"
"          0.302 Pervious Area"
"          80.000 Pervious length"
"          1.000 Pervious slope"
"          0.703 Impervious Area"
"          80.000 Impervious length"
"          1.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          75.000 Pervious SCS Curve No."
"          0.217 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          8.467 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.871 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.154 0.000 0.000 0.000 c.m/sec"
"          Catchment 101 Pervious Impervious Total Area "
"          Surface Area 0.302 0.703 1.005 hectare"
"          Time of concentration 46.973 5.306 9.318 minutes"
"          Time to Centroid 171.845 105.859 112.213 minutes"
"          Rainfall depth 40.417 40.417 40.417 mm"
"          Rainfall volume 121.86 284.33 406.19 c.m"
"          Rainfall losses 31.666 5.213 13.149 mm"
"          Runoff depth 8.751 35.204 27.268 mm"
"          Runoff volume 26.38 247.66 274.04 c.m"
"          Runoff coefficient 0.217 0.871 0.675 "
"          Maximum flow 0.005 0.154 0.154 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4  Add Runoff "
"          0.154 0.154 0.000 0.000"
" 54      POND DESIGN"
"          0.154 Current peak flow c.m/sec"
"          0.078 Target outflow c.m/sec"
"          274.0 Hydrograph volume c.m"

```

```

"      11.  Number of stages"
"      0.000  Minimum water level  metre"
"      1.500  Maximum water level  metre"
"      0.000  Starting water level  metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"      Level Discharge  Volume"
"      0.000  0.000  0.000"
"      0.1500  1.00E-07  33.000"
"      0.3000  1.00E-07  66.000"
"      0.4500  1.00E-07  99.000"
"      0.6000  0.01027  132.000"
"      0.7500  0.03866  165.000"
"      0.9000  0.05381  198.000"
"      1.050  0.06555  231.000"
"      1.200  0.07549  264.000"
"      1.350  0.08426  297.000"
"      1.500  0.09220  330.000"
(NOTE RATING CURVE DOES NOT REFLECT SITE DESIGN, ADDED FOR VOLUME ESTIMATES ONLY)
"      1.  ORIFICES"
"      Orifice  Orifice  Orifice Number of"
"      invert  coefficie  diameter  orifices"
"      0.450  0.630  0.2100  1.000"
"      Peak outflow  0.036  c.m/sec"
"      Maximum level  0.736  metre"
"      Maximum storage  162.017  c.m"
"      Centroidal lag  2.791  hours"
"      0.154  0.154  0.036  0.000 c.m/sec"

```

```

"          MIDUSS Output ----->"
"          MIDUSS version                Version 2.25 rev. 473"
"          MIDUSS created                 February 7, 2010"
"          10 Units used:                  ie METRIC"
"          Job folder:                    Z:\Project Files\PROJECTS\Fort Erie\
"          1127 Garrison Road, Fort Erie\SWM Calculations"
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"          Company                        LandSmith Engineering & Consulting Ltd."
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"          1500.000 Max. Hydrograph"
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"          1 Chicago storm"
"          1083.550 Coefficient A"
"          6.618 Constant B"
"          0.735 Exponent C"
"          0.500 Fraction R"
"          180.000 Duration"
"          1.000 Time step multiplier"
"          Maximum intensity              137.317 mm/hr"
"          Total depth                    69.634 mm"
"          6 005hyd Hydrograph extension used in this file"
" 33          CATCHMENT 101"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          101 No description"
"          70.000 % Impervious"
"          1.005 Total Area"
"          80.000 Flow length"
"          1.000 Overland Slope"
"          0.302 Pervious Area"
"          80.000 Pervious length"
"          1.000 Pervious slope"
"          0.703 Impervious Area"
"          80.000 Impervious length"
"          1.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          75.000 Pervious SCS Curve No."
"          0.368 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          8.467 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.914 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.266 0.000 0.000 0.000 c.m/sec"
"          Catchment 101 Pervious Impervious Total Area "
"          Surface Area 0.302 0.703 1.005 hectare"
"          Time of concentration 31.630 4.357 8.374 minutes"
"          Time to Centroid 150.490 102.985 109.981 minutes"
"          Rainfall depth 69.634 69.634 69.634 mm"
"          Rainfall volume 209.95 489.87 699.82 c.m"
"          Rainfall losses 43.998 6.021 17.414 mm"
"          Runoff depth 25.636 63.613 52.220 mm"
"          Runoff volume 77.29 447.52 524.81 c.m"
"          Runoff coefficient 0.368 0.914 0.750 "
"          Maximum flow 0.020 0.263 0.266 c.m/sec"
" 40          HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.266 0.266 0.000 0.000"
" 54          POND DESIGN"

```

```

"      0.266 Current peak flow c.m/sec"
"      0.078 Target outflow c.m/sec"
"      524.8 Hydrograph volume c.m"
"      11. Number of stages"
"      0.000 Minimum water level metre"
"      1.500 Maximum water level metre"
"      0.000 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.000"
"      0.1500 1.00E-07 33.000"
"      0.3000 1.00E-07 66.000"
"      0.4500 1.00E-07 99.000"
"      0.6000 0.01027 132.000"
"      0.7500 0.03866 165.000"
"      0.9000 0.05381 198.000"
"      1.050 0.06555 231.000"
"      1.200 0.07549 264.000"
"      1.350 0.08426 297.000"
"      1.500 0.09220 330.000"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      0.450 0.630 0.2100 1.000"
"      Peak outflow 0.076 c.m/sec"
"      Maximum level 1.208 metre"
"      Maximum storage 265.839 c.m"
"      Centroidal lag 2.586 hours"
"      0.266 0.266 0.076 0.000 c.m/sec"

```

## Appendix 'E'

---

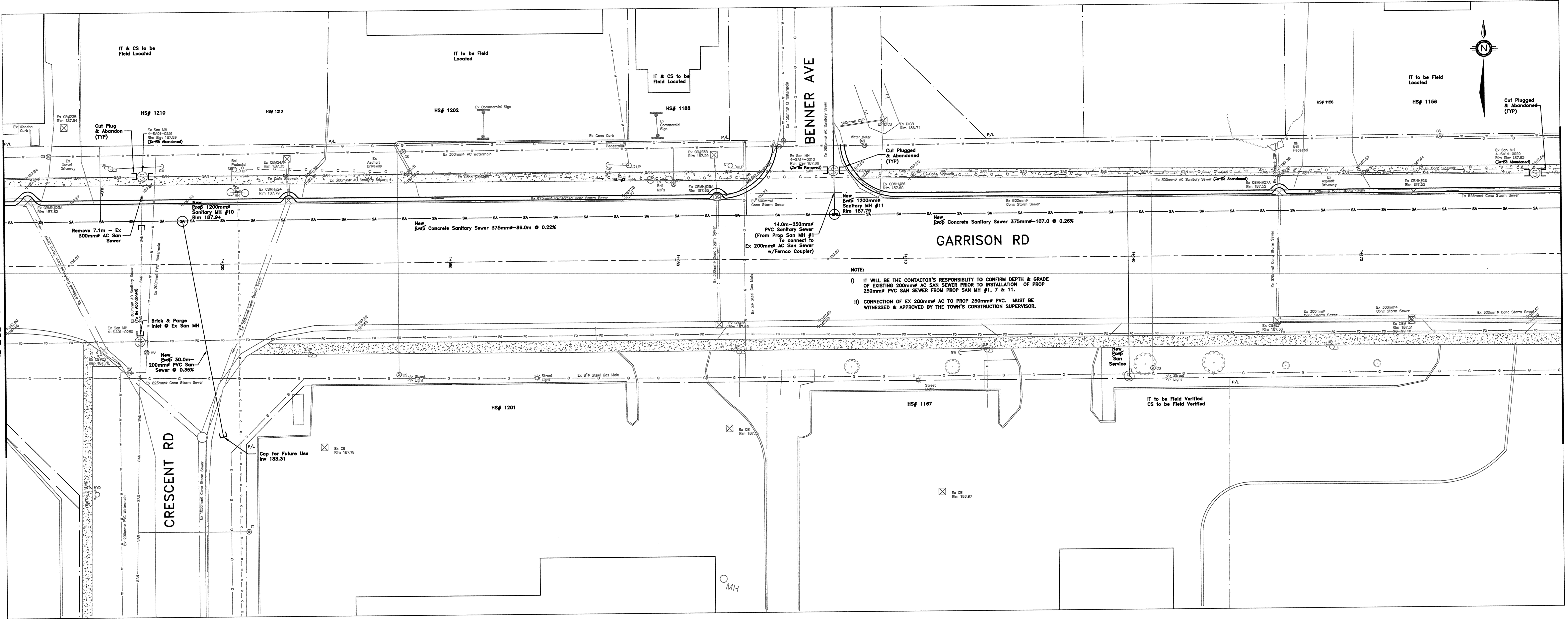
Garrison Road Plan & Profile, Sheet 6

Garrison Road Plan & Profile, Sheet 7

East Bertie Sewerage System Plan & Profile

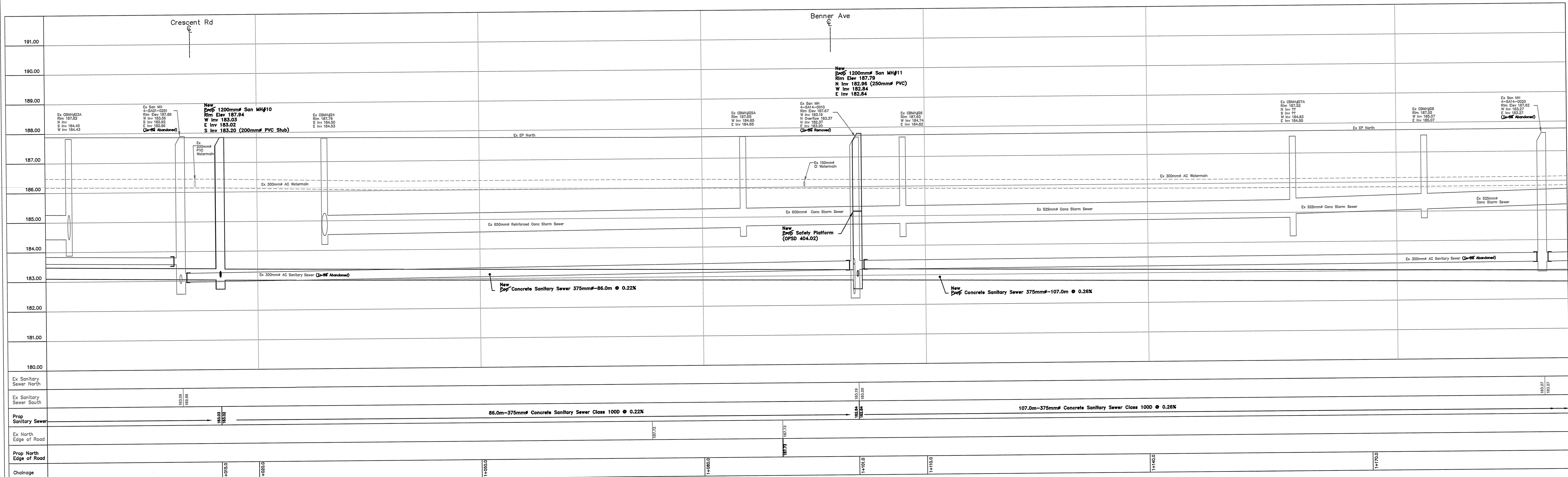
SEE SHEET 5 OF 10  
STA 0+991.5

SEE SHEET 7  
STA 1+196.5



NOTE:  
1) IT WILL BE THE CONTRACTOR'S RESPONSIBILITY TO CONFIRM DEPTH & GRADE OF EXISTING 300mm AC SAN SEWER PRIOR TO INSTALLATION OF PROP 250mm PVC SAN SEWER FROM PROP SAN MH #1, 7 & 11.  
2) CONNECTION OF EX 200mm AC TO PROP 250mm PVC MUST BE WITNESSED & APPROVED BY THE TOWN'S CONSTRUCTION SUPERVISOR.

# GARRISON ROAD



**LEGEND**

EXISTING		PROPOSED	
—	Sanitary Sewer	—	Sanitary Sewer
—	Watermain	—	Sanitary Inspection Tee
—	Gas Line	—	Concrete Curb
—	Edge of Asphalt Road	—	Sanitary Manhole
—	Bell Underground	—	
—	Bell Conduit		
—	Hydro Underground		
CB	Catch Basin	SB	Standard Iron Bar
WH	Wood Hydro Pole	IP	Iron Pipe
WLP	Wood Light Pole	GV	Gas Valve
IB	Iron Bar	NV	Water Valve
BP	Bell Pedestal	CS	Curb Stop
CC	Cut Cross	HYD	Hydrant
RB	Round Iron Bar	IT	Inspection Tee

REV.	ISSUE	DATE	BY
5	ISSUED FOR AS BUILT	JUNE 13, 2013	YR
4	ISSUED FOR CONSTRUCTION	AUG 31, 2011	SB
3	ISSUED FOR BIDDING	JULY 21, 2011	SB
2	ISSUED FOR TENDER	JULY 15, 2011	SB
1	ISSUED FOR REVIEW	JULY 7, 2011	SB

**BENCH MARK**

FROM INTERSECTION OF HWY 3 (GARRISON RD) AND THOMPSON RD, 0.14KM WEST TO GARRISON RD PUBLIC SCHOOL. CAP IS IN SOUTH FACE OF CONCRETE FOUNDATION IN EASTWARD PROJECTION, 36.80M NORTH OF CENTRE OF HWY 3, 0.30M WEST OF EASTERY CORNER. BM # V010890202 EASTING 698900 ELEVATION 188.281

**GARRISON ROAD SANITARY SEWER REPLACEMENT**

**FORT-ERIE** CONSULTANTS

SCALE: HORIZONTAL 1:200, VERTICAL 1:50

DATE: MAY 2011

PROJECT NO: IS10.GRSS

DWG. NO.: 6 OF 11

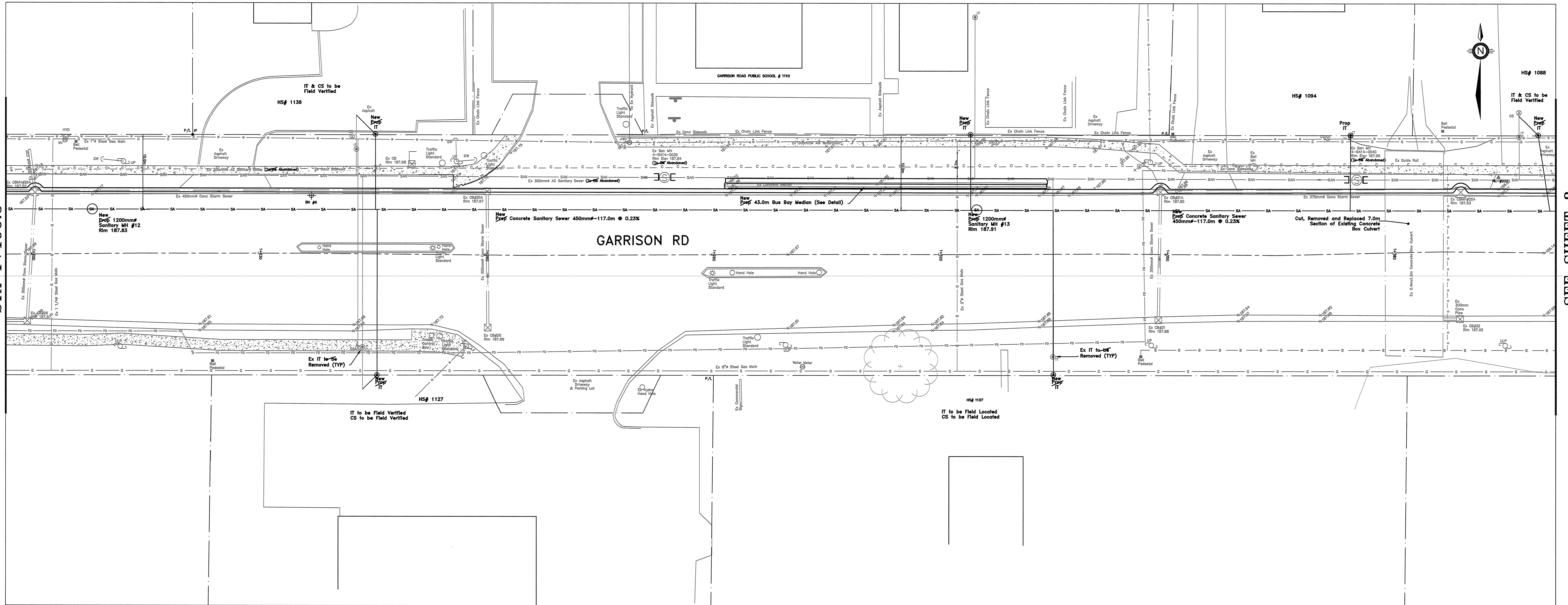
REV. 3

© V:\PROJECTS\Projects 2008\Garrison Rd Sanitary Sewer\CAD\Garrison Rd Phase 1 and 2-Isue for as built.dwg

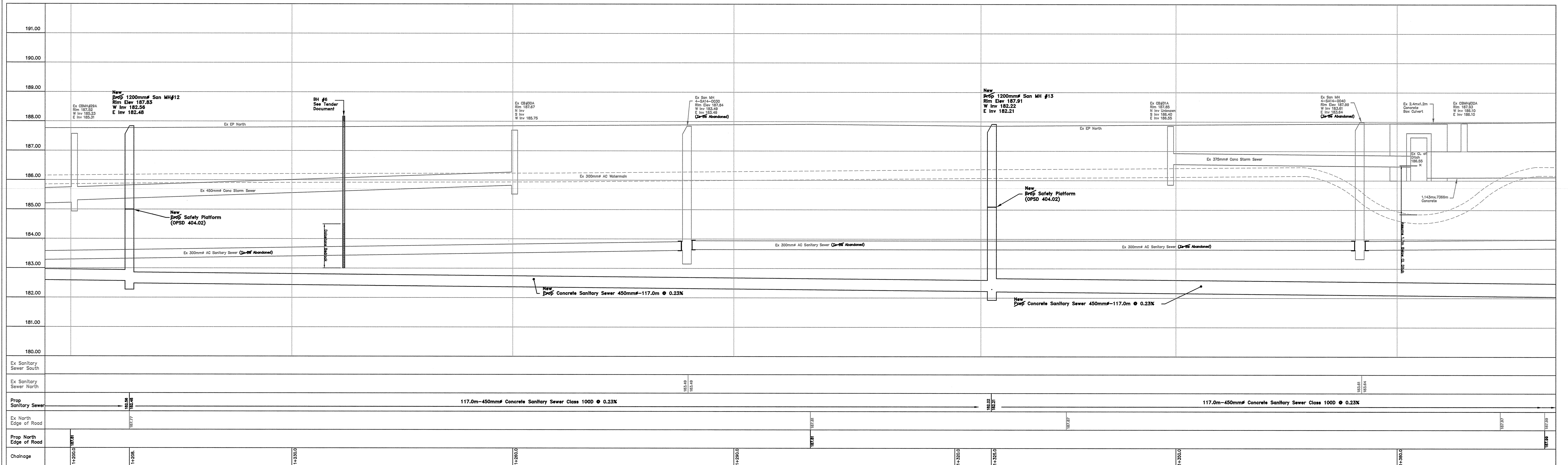


SEE SHEET 6 OF 10  
STA 1+196.5

SEE SHEET 8  
STA 1+401.5



# GARRISON ROAD



G:\PROJECTS\Projects 2008\Garrison Rd Sanitary Sewer\CAD\Garrison Rd Phase 1 and 2-issues for as building

EXISTING		PROPOSED	
—	Sanitary Sewer	—	Sanitary Sewer
—	Watermain	—	Sanitary Inspection Tee
—	Gas Line	—	Concrete Curb
—	Edge of Asphalt Road	—	Sanitary Manhole
—	Bell Underground		
—	Bell Conduit		
—	Hydro Underground		
CB	Catch Basin	IP	Iron Pipe
WHP	Wood Hydro Pole	GV	Gate Valve
IB	Iron Bar	WV	Water Valve
BP	Bell Pedestal	CS	Curb Stop
CC	Cut Cross	HYD	Hydrant
RB	Round Iron Bar	IT	Inspection Tee

REV.	ISSUE	DATE	BY
5	ISSUED FOR AS BUILT	JUNE 13, 2013	YR
4	ISSUED FOR CONSTRUCTION	AUG 31, 2011	SB
3	ISSUED FOR MDE	JULY 21, 2011	SB
2	ISSUED FOR TENDER	JULY 13, 2011	SB
1	ISSUED TO REVIEW	JULY 7, 2011	SB

BENCH MARK	
FROM INTERSECTION OF HWY 3 (GARRISON RD) AND THOMPSON RD, GO 1.40M WEST TO GARRISON RD PUBLIC SCHOOL. CAP IS IN SOUTH FACE OF CONCRETE FOUNDATION IN EASTWARD PROJECTION, 30.80M NORTH OF CENTRE OF HWY 3, 0.20M WEST OF EASTERY CORNER. BM # V01085202	
NORTHING	4752020
EASTING	686800
ELEVATION	188.281

Our Focus: Your Future

INFRASTRUCTURE SERVICES

**GARRISON ROAD**  
**SANITARY SEWER REPLACEMENT**

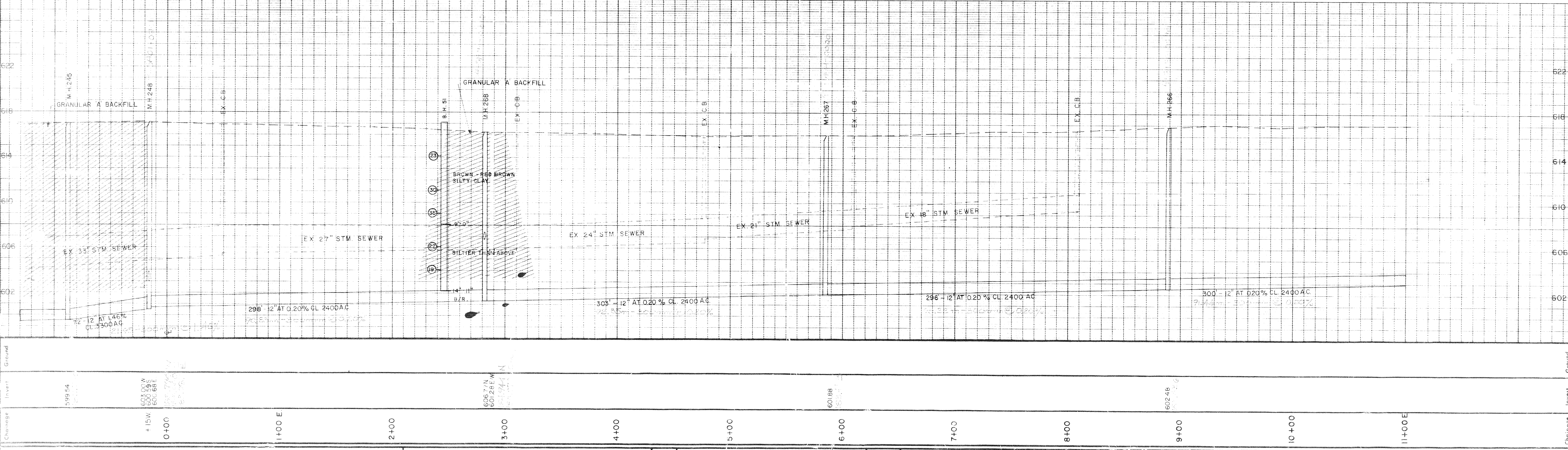
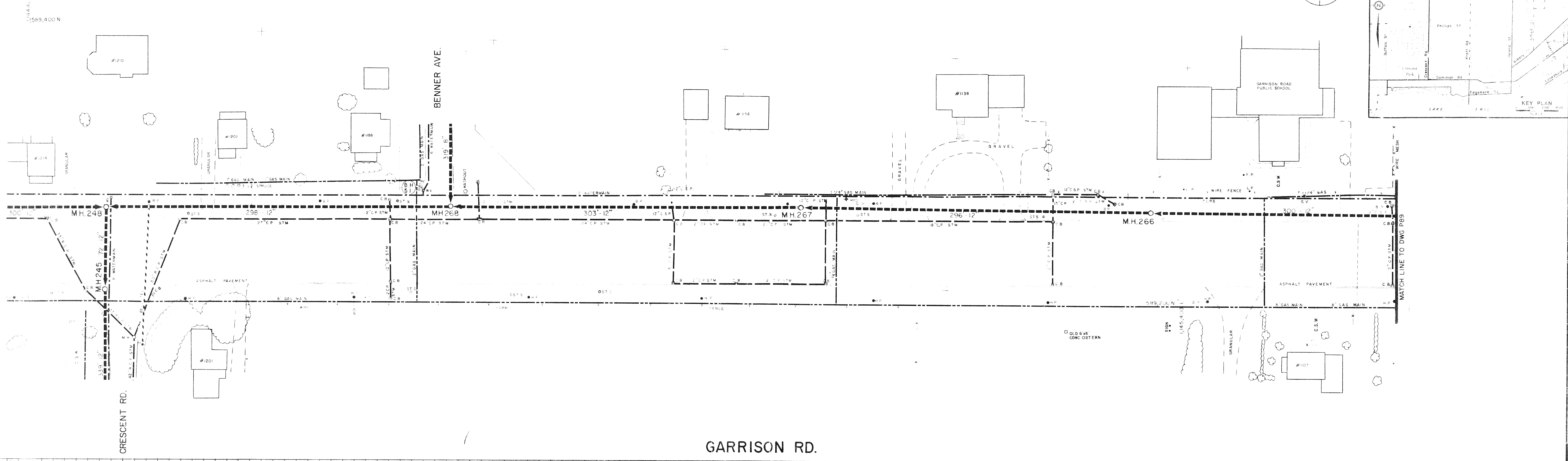
SCALE: HORIZONTAL 1:200, VERTICAL 1:50

DATE: MAY 2011

PROJECT NO. IS10.GRSS

DWG. NO. 7 OF 11

REV. 3



Notes: (1) FOR EXACT UTILITY LOCATIONS, CONSULT MUNICIPAL AUTHORITIES AND UTILITY COMPANIES CONCERNED.  
 (2) THE CONTRACTOR SHALL PROVE THE LOCATION OF UTILITIES AND SHALL BE RESPONSIBLE FOR ADEQUATE PROTECTION FROM DAMAGE.

No.	Revision	Date	Initial

Approved			
FINALIZED TO AS BUILT	SEPT 1973	W.S.	

Registered Professional Engineer  
**W. D. GOODINGS**  
 PROVINCE OF ONTARIO

TOWN OF FORT ERIE  
 EAST BERTIE SEWAGE WORKS AREA  
 GARRISON ROAD  
 CRESCENT RD. TO STA 11+00 E

**Proctor & Redfern Limited**  
 Consulting Engineers  
 Toronto St. Catharines

Scale Hor Vert 1" = 40' 1" = 40'  
 Date: JUNE 1971

Drawn: S.Y.O.L.S. Field Book Drawing No. 69584-PRB